







Document status

| Client | IPART |
|-----------------|---|
| Project | Sydney Aerotropolis - Mamre Road MUSIC Model Review |
| Report title | Final Report |
| Version | FINAL - B |
| Authors | Matthew Hardy |
| Project manager | Mathew Hardy |
| File name | IPR00002 - Sydney Aerotropolis - Mamre Road MUSIC Model Review - Final |
| Project number | IPR00002 |

Document history

| Version | Date issued | Reviewed by | Approved by | Sent to | Comment |
|--------------|-------------|----------------------|-------------|---------|--|
| DRAFT | 19/09/2024 | Alessandra Razera | N/A | N/A | Internal Draft for Review |
| FINAL - A | 20/09/2024 | N/A | N/A | IPART | Final Report |
| FINAL - B | 21/11/2024 | Matt Hardy | M Hardy | IPART | Final Report - Minor changes in response to Sydney Water's comments |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

Copyright and Limitation

This report has been produced by Hydrology and Risk Consulting Pty Ltd ACN 603 391 993 ("HARC") for IPART. Unless otherwise indicated, the concepts, techniques, methods and information contained within the report are the intellectual property of HARC and may not be reproduced or used in any form by third parties without the express written consent of HARC and IPART.

The report has been prepared based on the information and specifications provided to HARC by IPART. HARC does not warrant this document as being complete, current or free from error and disclaims all liability for any loss, damage, costs or expenses (including consequential losses) relating to this report. It should only be used for its intended purpose by IPART and should not be relied upon by third parties.

Copyright © Hydrology and Risk Consulting Pty Ltd ACN 603 391 993. All rights reserved.



Contents

| 1. | Introdu | uction | 1 |
|----|---------|--|------------|
| | 1.1 | Background | 1 |
| | 1.2 | About this review | 2 |
| | 1.2.1 | Objectives | 3 |
| | 1.2.2 | Scope | 3 |
| 2. | Mamr | e Road system modelling and design | 4 |
| | 2.1 | Background and context | 4 |
| | 2.2 | Modelling considerations | 5 |
| | 2.3 | Overview of the Sydney Water Modelling | 6 |
| | 2.4 | TWG reviews, findings and recommendations | 6 |
| | 2.4.1 | Background | 6 |
| | 2.4.2 | TWG's stormwater consultant findings and recommendations | 7 |
| 3. | Syster | m design comparison | 8 |
| | 3.1 | Northwest cluster | 8 |
| | 3.1.1 | Key elements of Sydney Water's design | 8 |
| | 3.1.2 | Differences in the TWG stormwater consultant's design | 8 |
| | 3.1.3 | Sydney Water's response to the TWG stormwater consultant changes | 9 |
| | 3.1.4 | Feasibility of designs | 9 |
| | 3.2 | East cluster | 10 |
| | 3.2.1 | Key elements of Sydney Water's design | 10 |
| | 3.2.2 | Differences in the TWG stormwater consultant's design | 10 |
| | 3.2.3 | Sydney Water's response to the TWG stormwater consultant changes | 11 |
| | 3.2.4 | Feasibility of designs | 11 |
| | 3.3 | Designs for meeting typical Sydney Metro local government 12 | targets |
| | 3.3.1 | Northwest cluster | 12 |
| | 3.3.2 | East cluster | 14 |
| | 3.4 | Water balance outcomes | 15 |
| 4. | Discus | ssion, findings and recommendations | 17 |
| | 4.1 | Discussion and findings | 17 |
| | 4.2 | Recommendations | 18 |
| 5. | Refere | ences | 19 |
| | Appen | idix A Technical requirements | 20 |
| | A.1 | Stormwater quantity targets | 20 |
| | A.2 | Wianamatta-South Creek Guidelines acceptable MUSIC treatment node 20 | parameters |
| | Appen | idix B MUSIC model details | 22 |
| | B.1 | MUSIC model schematics | 22 |
| | B.2 | MUSIC model inputs | 24 |
| | B.2.1 | Sydney Water Northwest Cluster | 24 |

IPR00002 - Sydney Aerotropolis - Mamre Road MUSIC Model Review - Final



| B.2.2 | TWG stormwater consultant Northwest Cluster Alternative 1 | 27 |
|-------|---|----|
| B.2.3 | Sydney Water East Cluster | 31 |
| B.2.4 | TWG stormwater consultant East Cluster Alternative 3 | 35 |
| B.3 | MUSIC model water balances | 39 |
| B.3.1 | Northwest cluster | 39 |
| B.3.2 | East cluster | 43 |



Executive Summary

The Mamre Road Precinct is a mixed green and brownfield industrial development located approximately 8 km northeast of the new Western Sydney International Airport (the Nancy-Bird Walton Airport) (Figure 1-1). The Precinct sits within the Wianamatta-South Creek corridor, immediately adjacent to the confluence of Kemps Creek and South Creek, bounded by Kemps Creek to the west and Ropes Creek to the east.

The NSW Governments' statutory and planning documents for the Aerotropolis and Mamre Road Precincts have adopted a new land-use planning and urban design approach to achieve the Parkland City vision for Western Sydney.

As part of this significant shift, new waterway health objectives and targets for the Wianamatta-South Creek Catchment have been set, based on the Risk-based Framework for Considering Waterway Health Outcomes in Strategic Land-use Planning Decisions. This framework has been applied in the development of targets, with the final targets outlined in the Wianamatta-South Creek stormwater management targets.

In early 2022, Sydney Water was appointed authority responsible for the management and delivery of stormwater management in the leading precincts. Sydney Water is responsible for designing, delivering, managing and maintaining the regional stormwater network in the precinct along with its drinking water, wastewater and recycled water systems.

In March 2024, the NSW Government asked IPART to provide advice on:

- i.) Determining the efficient costs of providing stormwater drainage services within the Mamre Road Precinct
- ii.) Allocating these costs efficiently between developers, taxpayers, and other stakeholders.

The stormwater management modelling for the Mamre Road precinct was undertaken using the Model for Urban Stormwater Improvement Conceptualisation (MUSIC). Hydrology and Risk Consulting (HARC) has been engaged by IPART to provide independent expert advice on the stormwater management system design and underlying MUSIC modelling to support its advice to the Government.

The objectives of this review were to advise IPART on:

- i. Whether the Mamre Rd precinct stormwater management system design:
 - (a) Complies with the relevant guidelines and standards and meets the mandated flow and water quality target for the region.
 - (b) Efficiently delivers the stormwater management services covered by the DSP charge.
- ii. In the context of system delivery:
 - (a) Which aspects of the design are the major drivers of cost, and what, if any, opportunities are there to reduce these costs?
 - (b) Which, if any, elements of the system should IPART's independent cost consultant focus on in their review of the delivery cost.



iii. Differences in the infrastructure requirements in meeting the new risk-based targets and those targets typically in place for Local Councils in the Greater Sydney region.

The scope of this project review includes the review of Sydney Water's MUSIC models and underlying conceptual design, particularly focusing on two of the five sub-catchment clusters, the Northwest and the East. The demand for recycled water used in the MUSIC modelling has been covered in other review work undertaken by IPART and is not in the scope of this review.

In September 2023, a technical working group (TWG) was created by DCCEEW to examine opportunities for optimising the Mamre Road stormwater scheme conceptual design. The TWG also included an independent stormwater management consultant who has provided specific advice and alternative concept design suggestions.

The TWG's stormwater consultant developed alternative designs for the two sub-catchment clusters, and these designs were used to compare with and contrast to Sydney Water's conceptual designs. In addition, the TWG provided other advice and recommendations from their review as consulted by IPART, and Sydney Water's response to this review is examined.

The new risk-based targets for Wianamatta-South Creek required greater levels of stormwater pollutant reduction than those typical targets set by local Councils in the Sydney Metropolitan area. These targets also include requirements for the management of flows.

The review of MUSIC modelling undertaken for the Northwest and East sub-catchment clusters for the Mamre Road development precinct has confirmed that the Sydney Water conceptual design produces predicted pollutant reduction and flow management outcomes that largely comply with the risk-based targets for the Wianamatta-South Creek.

The input pollutant load parameters used by Sydney Water for the different land uses comply with current industry standards.

The alternative conceptual layouts generated by the TWG stormwater consultant for the Northwest and East sub-catchment clusters also generate pollutant and flow outcomes that are largely compliant with the targets. The review information provided by the consultant includes valid suggestions for Sydney Water to consider in the ongoing improvement of their models.

The most significant potential impact on improving the efficiency of the Sydney Water concept design has been made by changing the configuration of treatment systems and increasing the depth of recycled water storage ponds. This results in a significant reduction in the footprint of treatment and stormwater recycling infrastructure. These will be major drivers of stormwater management system costs.

This result suggests that the efficiency of the Sydney Water conceptual design could be improved. It also suggests that Sydney Water's concept design approaches could be improved by examining a greater number of potential treatment and storage configurations and undertaking sensitivity testing of the concept design outcomes to changes in key assumptions and inputs.

In examining the information provided by Sydney Water and the MUSIC modelling files, it is apparent that the modelling and documentation could be improved with a more systematic approach to organising the modelling effort. This would include the adoption of procedures to



ensure consistent identification of model catchments, nodes and treatment and storage systems, plus the use of catchment imagery as a background for the positioning of treatment systems within the catchment.

The development of alternative conceptual layouts required to meet the typical Sydney Metropolitan pollution reduction standards demonstrates that the risk-based pollution reduction targets for Wianamatta-South Creek and the addition of flow management targets adds significantly to the size of treatment and storage systems and the associated area of land required.

This report makes the following recommendations:

- Sydney Water should consider the modification of their current conceptual design to incorporate the types of changes suggested in the alternative conceptual layouts developed by the TWG stormwater consultant across all five sub-catchment clusters.
- Given the importance of the demand for water in the sizing of recycled water storage ponds, Sydney Water should continue its efforts to better understand the likely demands for water in the types of large format industrial (LFI) development being developed in the Mamre Road precinct.
- 3. Sydney Water should develop formal internal procedures to support future MUSIC modelling efforts. These procedures should cover:
 - a. Model setup and organisation.
 - b. Treatment train optioneering.
 - c. Sensitivity testing.
- 4. Future stormwater modelling work in the Wianamatta-South Creek catchment should utilise an extended simulation time series.



1. Introduction

1.1 Background

The Mamre Road Precinct is a mixed green and brownfield industrial development located approximately 8 km northeast of the new Western Sydney International Airport (the Nancy-Bird Walton Airport) (Figure 1-1). The precinct sits within the Wianamatta-South Creek corridor, immediately adjacent to the confluence of Kemps Creek and South Creek, bounded by Kemps Creek to the west and Ropes Creek to the east.

The precinct falls in the land areas covered by the State Environmental Planning Policy (Western Sydney Employment Area) 2009 and is one of the Western Sydney Aerotropolis leading precincts.

The NSW Governments' statutory and planning documents for the Aerotropolis and Mamre Road Precincts have adopted a new land-use planning and urban design approach to achieve the Parkland City vision for Western Sydney.

As part of this significant shift, new waterway health objectives and targets for the Wianamatta-South Creek Catchment have been set, based on the Risk-based Framework for Considering Waterway Health Outcomes in Strategic Land-use Planning Decisions (Dela-Cruz, Pik, & Wearne, 2017). This framework has been applied in the development of flow and water quality targets, with the final targets outlined in the Wianamatta-South Creek stormwater management targets (Department of Planning and Environment, 2022b). These targets are now part of the Mamre Road Development Control Plan (DCP).

In late 2021, after the preparation of a Strategic Business Case (Frontier Economics, 2021) it was determined that a regional approach to the management of stormwater was the preferred approach to meeting the risk-based targets. Sydney Water was subsequently appointed the authority responsible for the management and delivery of stormwater management in the leading precincts. Sydney Water is responsible for designing, delivering, managing and maintaining the regional stormwater network in the precinct along with its drinking water, wastewater and recycled water systems.

In addition to the targets, the NSW Department of Climate Change, Energy, the Environment and Water (DCCEEW) released a number of important documents:

- *Review of water sensitive urban design strategies for Wianamatta–South Creek* (Department of Planning and Environment, 2022)
- *Technical guidance for achieving Wianamatta–South Creek stormwater management targets* (Department of Planning and Environment, 2022).

Sydney Water has been working towards its current conceptual design since later 2022. A series of iterations of the scheme have been released in draft form over that time.

In September 2023, a technical working group (TWG) was created by DCCEEW to examine opportunities for optimising the Mamre Road stormwater scheme conceptual design. The TWG also included an independent stormwater management consultant who provided specific advice and alternative concept design suggestions.





Figure 1-1 Mamre Road Precinct location in relation to the Western Sydney Aerotropolis (Sydney Water, 2021)

1.2 About this review

In March 2024, the NSW Government asked IPART to provide advice on:

- i.) Determining the efficient costs of providing stormwater drainage services within the Mamre Road Precinct.
- ii.) Allocating these costs efficiently between developers, taxpayers and other stakeholders.



Hydrology and Risk Consulting (HARC) has been engaged by IPART to provide independent expert advice on the stormwater management system design and underlying MUSIC modelling to support its advice to the Government.

1.2.1 Objectives

The objectives of this review were to advise IPART on:

- i. Whether the Mamre Rd precinct stormwater management system design:
 - (a) Complies with the relevant guidelines and standards and meets the mandated flow and water quality target for the region.
 - (b) Efficiently delivers the stormwater management services covered by the DSP charge.
- ii. In the context of system delivery:
 - (a) Which aspects of the design are the major drivers of cost, and what, if any, opportunities are there to reduce these costs?
 - (b) Which, if any, elements of the system should IPART's independent cost consultant focus on in their review of the delivery cost?
- iii. Differences in the infrastructure requirements in meeting the new risk-based targets and those targets typically in place for Local Councils in the Greater Sydney region.

1.2.2 Scope

This review has considered Sydney Water's MUSIC models (version 18) and the underlying treatment system design. It has focused on two of the five sub-catchment clusters modelled by SW, the Northwestern (NW) and the Eastern (E) clusters.

A review of the recycled stormwater demands used in the MUSIC model was outside the scope of this work but has been completed as part of separate review work undertaken by IPART.

The TWG's stormwater consultant developed alternative designs for these two subcatchment clusters, and these were compared and contrasted to Sydney Water's conceptual designs to develop recommendations for SW model improvements. Sydney Water's response to these recommendations is examined in this review..



2. Mamre Road system modelling and design

2.1 Background and context

Stormwater management within the Mamre Road precinct is governed by the Wianamatta-South Creek guidelines from the Department of Planning and Environment (DPE). These guidelines provide stormwater quantity and quality targets, design principles, and acceptable MUSIC model parameter ranges, as well as outline cost assumptions.

The stormwater quality reduction targets, shown in Table 2-1 are in mean annual load from unmitigated development. The Wianamatta-South Creek reduction targets are higher than the Penrith City and Blacktown City council targets, which are typical of those adopted by Local Councils throughout the Greater Sydney Metropolitan area. Further information on the guidelines is provided in Appendix A.

| Parameter | Wianamatta-South Creek Target (State of NSW and Department of Planning and Environment, 2022c) | Penrith City Council Targets (Penrith City Council, 2013) | Blacktown Council Targets (Blacktown City Council, 2020) | |
|------------------------------|--|--|---|--|
| Gross pollutants | 90% | 90% | 90% | |
| Total suspended solids (TSS) | 90% | 85% | 85% | |
| Total phosphorous (TP) | 80% | 60% | 65% | |
| Total Nitrogen | 65% | 45% | 45% | |

Table 2-1 Stormwater quality reduction targets

While the typical local Council has targets requiring the temporary detention of stormwater flow on-site to minimise the sizing of stormwater conveyance infrastructure and stream erosion, there are typically no targets for flow reductions across the fuller spectrum of flows. In contrast, the risk-based target for Wianamatta-South Creek includes the flow targets at different flow percentiles. Two options are provided for complying with the targets as shown in Table 2-2 and Table 2-3. With large areas of impervious surfaces in urban development, meeting these targets will necessitate the capture and re-use of some portion of stormwater flows.

Table 2-2 - Wianamatta-South Creek Flow Targets - Option 1

| Index | Target |
|--|-------------------------|
| Minimum Annual Runoff Volume (MARV) | < 2 ML/ha/yr |
| 90%ile | 1,000 to 5,000 L/ha/day |
| 50%ile | 5 to 100 L/ha/day |
| 10%ile | 0 L/ha/day |



| Index | Target |
|---------------|-----------------------------|
| 95%ile | 3,000 to 15,000 L/ha/day |
| 90%ile | 1,000 to 5,000 L/ha/day |
| 75%ile | 100 to 1,000 L/ha/day |
| 50%ile | 5 to 100 L/ha/day |
| Cease to Flow | 10-30% |

Table 2-3 - Wianamatta-South Creek Flow Targets - Option 2

2.2 Modelling considerations

The Model for Urban Stormwater Improvement Conceptualisation (MUSIC) simulates:

- Rainfall-runoff processes;
- Stormwater pollutant generation Total Suspended Solids (TSS), Total Phosphorus (TP), and Total Nitrogen (TN); and
- Pollutant removal by structural assets designed to manage and mitigate the hydrological and water quality impacts of urbanisation.

Consistent with modelling best practice, it is important to understand and interpret music modelling results in the context of the uncertainties inherent in the data, modelling assumptions and capabilities and limitations of the model itself.

Imteaz et al. (2013), Watson (2014) and Sydney Water's (2024a) all highlight the uncertainties associated with MUSIC modelling, in particular, those associated with the use of default model parameterisations (as is the case with the MUSIC models reviewed in this project).

Consequently, a modelling investigation needs to explore and understand the sensitivity of model results to key assumptions and input parameters and data.

To this end, HARC notes that the MUSIC models reviewed have been run using the comparatively short ten-year rainfall time series (1999-2008) specified for use in the Winematta Creek Guidelines (Department of Planning and Environment, 2022a). In the context of the full climate record (Figure 2-1), the rainfall period adopted is one of the drier periods on record.

While this rainfall period is suitable for evaluating the guideline specified flow and water quality objectives, caution should be exercised when evaluating other climate-related performance objectives such as stormwater reuse.





Figure 2-1 - Historical climate context - Mamre Road development precinct

2.3 Overview of the Sydney Water Modelling

Sydney Water's Mamre Road precinct MUSIC modelling consists of five separate MUSIC models built for each of the precinct's sub-catchments and referred to as the North, Northwest, East, West, and Southwest cluster models.

Sydney Water's MUSIC models incorporated the simulation of stormwater management devices such as gross pollutant traps, passively watered street trees, precinct bioretention basins and wetlands, as well as regional re-use storage in the form of ponds. These are all stormwater measures adopted in the WSUD strategies from the Wianamatta-South Creek guidelines (State of NSW and Department of Planning and Environment, 2022a).

Both the Northwest and East cluster models largely achieved the Wianamatta-South Creek water quality and quantity targets. In testing whether the models passed the water quality and quantity targets, two different nodes were checked. For water quality, the node at the end of the development (either South Creek or Ropes Creek nodes) was used. For water quantity, the flows were measured from the next node (labelled junction in both models), which also included flows from the area of public open space (POS) immediately adjacent to the receiving water bodies. This approach is justifiable as the flow targets are set for the entire catchment and this external POS will contribute.

2.4 TWG reviews, findings and recommendations

2.4.1 Background

In February 2024, the TWG stormwater consultant reviewed both the technical aspects of the scheme design and the costing from Sydney Water's (SW) updated December 2023 scheme. This included a review of the SW's assumptions used in their MUSIC and the development of Sydney Aerotropolis - Mamre Road MUSIC Model Review



alternative conceptual layouts for two of the five sub-catchment clusters (Northwest and East). Their costing review only assessed CAPEX and not OPEX.

2.4.2 TWG's stormwater consultant findings and recommendations

The TWG stormwater consultant found SW information to be below the required level for stormwater strategies submitted as part of State Significant Development (SSD) applications in NSW, with much of the information missing or difficult to interpret. Additionally, they found errors and efficiencies in the layout of SW's scheme in two of the five sub-catchment clusters examined.

The main issues raised by the TWG stormwater consultant as well as commentary on their context of good/best practice modelling are:

- Pond depths were shallow The Wianamatta Creek guidelines recommend a maximum pond depth of 3m. All of the TWG stormwater consultant's pond depths are within this range.
- Unrealistic drainage paths.
- Deep transfer pipes.
- Modelling not reflecting proposed configuration.
- Splitting flows upstream of wetlands.
- Ponds in powerline easement.
- Wetland only treatments the opportunity to reduce area of measures if coupled with bioretention
- Powerline easement not modelled separately.
- Reuse demand outlined in the Technical Guidelines were not adopted.
- Kemps Creek dam site is not considered.



3. System design comparison

Within the TWG stormwater consultant's review, four MUSIC models were created for both the NW and E clusters. Each model represented a design alternative. In this comparison, the Alternative 1 model from the NW cluster and the Alternative 3 model from the E cluster were focused on as they were assessed as the most comparable to SW's models. In the TWG stormwater consultant's alternatives, they proposed deeper, consolidated, reshaped ponds, coupled bioretention and wetland treatments, different reuse demands, and other changes within the MUSIC models and WSUD system. They also raised the possibility of using Kemps Creek dam in the NW cluster, and a turkey nest dam in the E cluster. These last two options were not considered in our assessment due to time constraints.

Both the alternative models that were compared largely achieved the Wianamatta-South Creek water quality and quantity targets. Similarly to the SW models, the water quality was tested at the penultimate node, and water quality at the final node.

In the TWG stormwater consultant's model, small adjustments in water demand were made to reflect changes in the land available for POS irrigation due to reductions in treatment system footprints.

3.1 Northwest cluster

3.1.1 Key elements of Sydney Water's design

- Three catchments: NW01, NW02 and NW03.
- Each catchment has three lot source nodes: Roof, Pavement, and Landscape. All flow into a Gross Pollutant Trap (GPT).
- Each catchment has two street nodes: Pervious and Pavement. Both flow into the bioretention street trees.
- In NW01 and NW02, the GPT and bioretention street trees both flow into a bioretention.
 In NW03 there is also a Wetland with an inlet pond, with weir overflow which then flows into a bioretention.
- In all the catchments, this then runs into a Pond (1 for NW01, and 2 + 3 for NW02 and NW03). IN NW02 there is a generic treatment node that diverts flows less than 0.0125m³/s around the pond directly to Wianamatta-South Creek.
- NW01 also has some POS which flows directly into Pond 1.
- From the ponds, the flow goes to Wianamatta-South Creek.
- All the ponds have re-use.
- There is also some flow from external POS which goes to a node beyond Wianamatta-South Creek.

3.1.2 Differences in the TWG stormwater consultant's design

 Sedimentation Basins are added before the bioretentions in NW01 and NW03, and before the wetland in NW02. These replace either the inlet pond volume in the wetland, or filter area in the bioretentions. The TWG stormwater consultant sedimentation pond in



NW02 is reduced in size from the size of the inlet pond volume in SW's model ($2970m^3 - 1500m^3$).

- Pond 1 is removed. The depth of Pond 2 + 3 is increased to 2.999m from 1.755m. The surface area is consequently decreased. However, the TWG stormwater consultant's volume in Pond 2 + 3 is still greater than the combined pond volumes in SW's model (165,000m³ compared to 134,882m³)
- The total monthly pattern re-use was increased slightly.
- The internal POS in NW01 is routed through the bioretention in NW01.
- Several areas in the model were decreased or increased in both source and treatment nodes.
- The differences in the stormwater water balance outcomes between the two models is discussed in Section 3.4.

3.1.3 Sydney Water's response to the TWG stormwater consultant changes

In a TWG paper, Sydney Water (2024b) provided the following responses to the design improvement suggestions:

- The sedimentation basins were initially modelled as part of other nodes as it was easier during the scheme planning to reduce number of changes. Moving forward SW may separate sedimentation basins into separate nodes as scheme progresses.
- In response to the pond changes, SW is open to further deepening ponds and are currently undertaking investigations into feasibility. They will also review the pond shapes during the detail design to ensure efficiency.
- SW will continue to use their recycled water demands because if the predicted demands are not achieved, they will breach stormwater quantity targets.

3.1.4 Feasibility of designs

The MUSIC model parameters were compared to the acceptable parameter ranges and design principles from the Technical guidance for achieving Wianamatta-South Creek stormwater management targets (State of NSW and Department of Planning and Environment, 2022b). The following discrepancies were found in SW's models:

- The total nitrogen (TN) content of filter media was 400 mg/kg in all bioretention basins and street trees, compared to the acceptable value of 800mg/kg.
- There was no pre-treatment sedimentation basin or wetland for the bioretention basins in catchment NW01 or NW02.
- The permanent pool volume in the wetland in the NW03 catchment was outside the acceptable range of 0.3 – 0.4 m times wetland surface area (instead 0.28)
- The notional detention time for the wetland in NW03 was 47.9hrs, which is below the acceptable minimum of 48hrs. Due to the uncertainty in MUSIC model parameters, although this falls outside the acceptable range provided, it is close enough to not cause concern.



In the TWG stormwater consultant's model sedimentation basins were added before the bioretention basins in the NW01 and NW02 catchments, and the permanent pool volume was within the acceptable range. However, the TN content and notional detention time values remained the same.

3.2 East cluster

3.2.1 Key elements of Sydney Water's design

- Three catchments: E01, E02, and E03.
- Each catchment has three lot source nodes: Roof, Pavement, and Landscape. All flow into a Gross Pollutant Trap (GPT).
- Each catchment has two street nodes: Pervious and Pavement. Both flow into the bioretention street trees.
- In all the catchments, the GPT and bioretention street trees flow into a wetland. The weir overflow then flows into a pond in each catchment. In E03 there is also a bioretention, that the weir overflow flows into from the wetland, then to the pond.
- The outflows from the wetland as well as the outflows from the ponds, flow into Ropes creek.
- All the ponds have re-use.
- There is also some flow from external POS which goes to a node beyond Ropes creek.

3.2.2 Differences in the TWG stormwater consultant's design

- The depth of all the ponds was increased to 2m. The surface area is consequently decreased, with a slight decrease in total volume (112,410m³ to 100,356m³). The impervious fraction (IF) of Pond 29 + 30 + 31 in E03 was decreased from 100% to 90% to match the IF of the other ponds.
- The daily re-use demands were decreased at all ponds.
- The wetland source and treatment areas were changed in all catchments. The IF in wetland 25 + 26 (E01) and 28 (E02) source nodes was decreased from 90% to 40% to match the IF in wetland 29 + 30 + 31 (E03). Other input changes were also made to all three wetlands.
- Bioretention nodes were added in E01 and E02 after the wetlands to create coupled systems. All outflow except for the pipe flow from these new bioretention nodes is directed straight to Ropes creek. The pipe flow flows to the ponds. There were also changes in source and treatments areas.
- The TWG stormwater consultant modelled the easements separately. Creating a separate source node for each catchment with an IF of 20%. Consequently, the lot areas in all three catchments were decreased by this same amount. In each catchment they were proportionally split across the three contributing nodes, roof, pavement and landscape.
- A gained area source node was added, with an area similar to the reduction in area required for treatments in the cluster. This has an IF of 20%.



• The differences in the stormwater water balance outcomes between the two models is discussed in Section 3.4.

3.2.3 Sydney Water's response to the TWG stormwater consultant changes

In a TWG paper, Sydney Water (2024b) provided the following responses to the design improvement suggestions:

- In response to the pond changes, SW is open to further deepening ponds and are currently undertaking investigations into feasibility. They will also review the pond shapes during the details design to ensure efficiency.
- SW will continue to use their recycled water demands because if the predicted demands are not achieved, they will breach stormwater quantity targets.
- In reference to the coupled bioretention-wetland systems, the developers pipe grades are insufficient to accommodate biofiltration. Further refinement of the scheme is ongoing.
- SW will model the easements separately in the next revision of MUSIC models if beneficial to do so. In the initial model it was easier to model the easements together to reduce the number of changes.

3.2.4 Feasibility of designs

The MUSIC model parameters were compared to the acceptable parameters ranges and design principles from the Technical guidance for achieving Wianamatta-South Creek stormwater management targets (State of NSW and Department of Planning and Environment, 2022b). The following discrepancies were found in SW's models:

- The total nitrogen (TN) content of filter media was 400 mg/kg in all bioretention basins and street trees, compared to the acceptable value of 800mg/kg.
- The permanent pool volume in the wetland in all the catchments was outside the acceptable range of 0.3 0.4 m times wetland surface area (instead 0.13, 0.14, and 0.28).
- The notional detention time for the wetlands in E01 and E02 were 47.9 and 47.6hrs respectively, which is below the acceptable minimum of 48hrs. Due to the uncertainty in MUSIC model parameters, although this falls outside the acceptable range provided, it is close enough to not cause concern.
- The unlined filter media perimeter in the bioretention basin in E03 was 14m compared to the acceptable range of 0.01m.

In the TWG stormwater consultant's model the wetlands' permanent pool volumes were within the acceptable range, and the unlined filter media perimeter in the bioretention were set to the acceptable value of 0.01m. However, the TN content and notional detention time values remained outside the acceptable ranges.



3.3 Designs for meeting typical Sydney Metro local government targets

Additional MUSIC models were created for the Northwest and East clusters that satisfied typical flow quality targets in place in local government areas across the Sydney Metropolitan area. The purpose was to understand the impacts of the higher flow quality targets set in the Wianamatta-South Creek guidelines on infrastructure requirements.

The water quality standards adopted as typical for local government are set out Table 3-1.

 Table 3-1 - Assumed typical Sydney Metropolitan local Council stormwater quality reduction targets

| Parameter | Reduction target |
|------------------------------|------------------|
| Gros pollutants | 90% |
| Total suspended solids (TSS) | 85% |
| Total phosphorous (TP) | 60% |
| Total Nitrogen | 45% |

The designs provided by the TWG stormwater consultant were further modified to meet the less stringent standards typically applied by local councils in the Sydney Metropolitan area. The storage ponds and water recycling elements were removed from the conceptual layouts as the on-site detention of water is required under all targets. The changes in the sizing of treatment and storage nodes associated with all designs, including those required to meet typical Sydney Metropolitan Council targets is shown in Table 3-2 to Table 3-8.

3.3.1 Northwest cluster

Table 3-2 - Design parameters - Northwest cluster - Bioretention

| Basin No.: | | 1 | | | 2 | | | 3 | |
|-----------------------------------|-----------------------------|------------|-------------------------|--|--------------------|------------------------------------|---|--------------|------------------------|
| Treatment node: | Altis_Bioretention Nth | | NW02_Bioretention | | tion A | Altis_Bioretention Sth | | on Sth | |
| Parameter: | Surf ace Area (m²) | EDD (m) | Filter dept h (m) | Surf E ace (Area (m ²) | EDD F m) c ł | Filter S dept a n (m) A (| Surf El Ice (m Area m ²) | DD 1) (| Filter depth (m) |
| Sydney Water Design | 1,406.0 | 0.30 | 0.50 | 4,186.0 | 0.30 | 0.50 | 4,709.0 | 0.30 | 0.50 |
| TWG Consultant Design | 1,006.0 | 0.30 | 0.50 | 3,500.0 | 0.30 | 0.50 | 2,500.0 | 0.30 | 0.50 |
| Typical Council Targets Design | 1,156.9 | 0.30 | 0.50 | 4,025.0 | 0.30 | 0.50 | 2,875.0 | 0.30 | 0.50 |



Table 3-3 - Design parameters - Northwest cluster - Wetlands

| Basin No.: | | 1 | |
|-----------------------------------|-------------------------|--------------|--|
| Treatment node: | | Wetland 4 | |
| Parameter: | Surface Area (m²) | Depth (m) | Inlet pond volume (m ³) |
| Sydney Water Design | 9,575.0 | 0.28 | 2,970.0 |
| TWG Consultant Design | 9,575.0 | 0.30 | 0.0 |
| Typical Council Targets Design | 9,575.0 | 0.30 | 0.0 |

Table 3-4 - Design parameters - Northwest cluster - Sedimentation basins

| Basin No.: | | 1 | 2 | | 4 | |
|--------------------------|-------------------------|-----------------|-------------------------|-----------------------------------|------------------------|--------------|
| Treatment node: | Sedime Ba | entation sin | Sedimentation Basin | | Sedimentation Basin | |
| Parameter: | Surface Area (m²) | Depth (m) | Surface Area (m²) | Surface Depth Area (m) (m²) | | Depth (m) |
| Sydney Water Design | N/A | N/A | N/A | N/A | N/A | N/A |
| TWG Consultant Design | 400.0 | 1.50 | 500.0 | 1.50 | 1,000.0 | 1.50 |
| Typical Council | 400.0 | 1.50 | 500.0 | 1.50 | 1,000.0 | 1.50 |

Table 3-5 - Design parameters - Northwest cluster - Ponds

| Basin No.: | | 1 | 2 | |
|-----------------------------------|-------------------------|--------------|-------------------------|--------------|
| Treatment node: | Por | nd 1 | + Pond 3 | |
| Parameter: | Surface Area (m²) | Depth (m) | Surface Area (m²) | Depth (m) |
| Sydney Water Design | 10,323.0 | 1.79 | 66,324.0 | 1.76 |
| TWG Consultant Design | N/A | N/A | 55,000.0 | 3.00 |
| Typical Council Targets Design | N/A | N/A | N/A | N/A |



3.3.2 East cluster

Table 3-6 - Design parameters - East cluster - Bioretention

| Basin No.: | | 25 + 26 | | | 28 | | 29 + 30 + 31 | | | | |
|-----------------------------------|--------------------------|------------|-------------------------|-----------------------------|------------|-------------------------|-----------------------------|------------|------------------------|--|--|
| Treatment node: | 2 | 5-26 Bic |) | | 28 Bio | | E03_Bioretention | | | | |
| Parameter: | Surfac e Area (m²) | EDD (m) | Filter dept h (m) | Surf ace Area (m²) | EDD (m) | Filter dept h (m) | Surf ace Area (m²) | EDD (m) | Filter depth (m) | | |
| Sydney Water Design | N/A | N/A | N/A | N/A | N/A | N/A | 8,176.0 | 0.30 | 0.50 | | |
| TWG Consultant Design | 1,731.0 | 0.30 | 0.50 | 822.0 | 0.30 | 0.50 | 6,707.0 | 0.30 | 0.50 | | |
| Typical Council Targets Design | 1,731.0 | 0.30 | 0.50 | 822.0 | 0.30 | 0.50 | 6,707.0 | 0.30 | 0.50 | | |

Table 3-7 - Design parameters - East cluster - Wetlands

| Basin No.: | | | | 28 | | 29 + 30 + 31 | | | | |
|-----------------------------------|--------------------------|------------------|----------------------------------|--------------------------|------------------|---|-----------------------------|------------------|--|--|
| Treatment node: | Wet | land 25 | + 26 | W | etland | 28 | Wetland 29 + 30 + 31 | | | |
| Parameter: | Surfac e Area (m²) | Dept h (m) | Inlet pond volum e (m³) | Surfac e Area (m²) | De pth (m) | Inlet pond volum e (m ³) | Surfa ce Area (m²) | Dep th (m) | Inlet pond volu me (m ³) | |
| Sydney Water Design | 6,005.7 | 0.13 | 2,751.8 | 3,357.5 | 0.14 | 1,542.2 | 22,962 | 0.28 | 5,727.0 | |
| TWG Consultant Design | 5,193.0 | 0.33 | 1,154.0 | 2,466.0 | 0.33 | 548.0 | 20,122 | 0.33 | 4,472.0 | |
| Typical Council Targets Design | 5,193.0 | 0.33 | 1,154.0 | 2,466.0 | 0.33 | 548.0 | 20,122 | 0.33 | 4,472.0 | |

Table 3-8 - Design parameters - East cluster - Ponds

| Basin No.: | 25 + 2 | 26 | 28 | | 29 + 30 + 31 | | | |
|-----------------------------------|----------------------|--------------|----------------------|--------------|----------------------|--------------|--|--|
| Treatment node: | Pond 25 | + 26 | Pond | 28 | Pond 29 + 30 + 31 | | | |
| Parameter: | Surface Area (m²) | Depth (m) | Surface Area (m²) | Depth (m) | Surface Area (m²) | Depth (m) | | |
| Sydney Water Design | 14,904.0 | 1.82 | 5,440.7 | 1.25 | 49,983.0 | 1.57 | | |
| TWG Consultant Design | 12,216.0 | 2.00 | 2,961.0 | 2.00 | 35,000.0 | 2.00 | | |
| Typical Council Targets Design | N/A | N/A | N/A | N/A | N/A | N/A | | |



3.4 Water balance outcomes

Figure 3-1 and Figure 3-2 summarise the system water balance for the Northwest and Eastern clusters. A more detailed breakdown of these water balances can be found in Appendix B.

The figures show

- The SW and TWG stormwater consultant conceptual layouts achieve similar outcomes.
- The importance of stormwater harvesting in managing the runoff volume and achieving the flow reduction targets.

The observed difference in the evaporative losses between the SW and TWG layouts was investigated and found to be a function of land use classification; being driven by differences in the proportion of imperviousness and treatment pond surface area and the relative differences in the evaporation rates of these landuses.



Figure 3-1 - Water balance outcomes - Northwest cluster





Figure 3-2 - Water balance outcomes - East cluster



4. Discussion, findings and recommendations

4.1 Discussion and findings

The review of MUSIC modelling undertaken for the Northwest and East sub-catchment clusters for the Mamre Road development precinct has confirmed that the Sydney Water conceptual design produces predicted pollutant reduction and flow management outcomes that largely comply with the risk-based targets for the Wianamatta-South Creek.

The input pollutant load parameters used by Sydney Water for the different land uses comply with current industry standards.

The alternative conceptual layouts generated by the TWG stormwater consultant for the Northwest and East sub-catchment clusters also generate pollutant and flow outcomes that are largely compliant with the targets. The review information provided by the consultant includes valid suggestions for Sydney Water to consider in the ongoing improvement of their models.

The most significant potential impact on improving the efficiency of the Sydney Water concept design has been made by changing the configuration of treatment systems and increasing the depth of recycled water storage ponds. This results in a significant reduction in the footprint of treatment and stormwater recycling infrastructure. These will be major drivers of stormwater management system costs.

This result suggests that the efficiency of the Sydney Water conceptual design could be improved. This result also suggests that Sydney Water's concept design approaches could be improved by examining a greater number of potential treatment and storage configurations and also undertaking sensitivity testing of the concept design outcomes to changes in key assumptions and inputs.

In examining the information provided by Sydney Water and the MUSIC modelling files, it is apparent that the modelling and documentation could be improved with a more systematic approach to organising the modelling effort. This would include the adoption of procedures to ensure consistent identification of model catchments, nodes, treatment and storage systems, plus the use of catchment imagery as a background for the positioning of treatment systems within the catchment.

The development of alternative conceptual layouts required to meet the typical Sydney Metropolitan pollution reduction standards, demonstrates that the risk-based pollution reduction targets for Wianamatta-South Creek and the addition of flow management targets adds significantly to the size of treatment and storage systems and the associated area of land required. Sydney Aerotropolis - Mamre Road MUSIC Model Review Final Report



4.2 Recommendations

This report makes the following recommendations:

- Sydney Water should consider the modification of its current conceptual design to incorporate the types of changes suggested in the alternative conceptual layouts developed by the TWG stormwater consultant across all five sub-catchment clusters.
- Given the importance of the demand for water in the sizing of recycled water storage ponds, Sydney Water should continue its efforts to better understand the likely demands for water in the types of large-format industrial development being developed in the Mamre Road precinct.
- 3. Sydney Water should develop formal internal procedures to support future MUSIC modelling efforts. These procedures should cover:
 - a. Model setup and organisation.
 - b. Treatment train optioneering.
 - c. Sensitivity testing.
- 4. Future stormwater modelling work in the Wianamatta-South Creek catchment should utilise an extended simulation time series.



5. References

Blacktown City Council (2020). *WSUD developer handbook - MUSIC modelling and design guide.*

Dela-Cruz, J., Pik, A., & Wearne, P. (2017). Risk-based framework for considering waterway health outcomes in strategic land-use planning decisions. Sydney: Office of Environment and Heritage and Environmental Protection Authority.

DesignFlow (2023). *Guidance for Optimising Regional Stormwater Infrastructure – Western Sydney.*

Frontier Economics. (2021). Governance of stormwater and waterways in Wianamatta-South Creek (Leading Precincts)

Imteaz et al. (2013), 'Modelling stormwater treatment systems using MUSIC: Accuracy', *Resources, Conversation and Recycling*, 71: 15-21

Penrith City Council (2013). Water Sensitive Urban Design (WSUD) Policy.

State of NSW and Department of Planning and Environment (2022a). *Review of water* sensitive urban design strategies for Wianamatta-South Creek. Paramatta

State of NSW and Department of Planning and Environment (2022b). *Technical guidance for achieving Wianamatta-South Creek stormwater management targets*. Paramatta

State of NSW and Department of Planning and Environment (2022c). *Wianamatta-South Creek stormwater management targets*. Paramatta

Sydney Water (2021). Mamre Road Precinct Integrated Water Cycle Management Strategy.

Sydney Water (2024a). *Green infrastructure stormwater retention performance report – Stage 2 calibration*. Version 1.2

Sydney Water (2024b) Mamre Road Technical Working Group (TWG) - Optimised Regional Stormwater Infrastructure - Risks, opportunities, and other considerations paper

Watson T. D. (2014), *MUSIC Stormwater Modelling: A Calibration Study*, University of Melbourne.



Appendix A Technical requirements

A.1 Stormwater quantity targets

Table A-1: Wianamatta-South Creek Operational phase stormwater quantity (flow) targets Option 1 – MARV (State of NSW and Department of Planning and Environment, 2022c)

| Parameter | Target |
|----------------------------------|--|
| Mean annual runoff volume (MARV) | $\leq\!\!2$ ML/ha/y at the point of discharge to the local waterway |
| 90%ile flow | 1,000–5,000 L/ha/day at the point of discharge to the local waterway |
| 50%ile flow | 5–100 L/ha/day at the point of discharge to the local waterway |
| 10%ile flow | 0 L/ha/day at the point of discharge to the local waterway |

A.2 Wianamatta-South Creek Guidelines acceptable MUSIC treatment node parameters

Table A-2: Parameter ranges for sedimentation basins (State of NSW and Department of Planning and Environment, 2022b)

| Sedimentation basin | Acceptable parameter ranges |
|--------------------------|--|
| Surface area | User defined |
| Extended detention depth | Maximum extended detention depth of 350 mm when part of a wetland system and up to 1.0 m when acting in isolation |
| Permanent pool volume | Calculate with depth up to a maximum of 2.0 m |
| Initial volume | Same as permanent pool volume |
| Exfiltration rate | Maximum of 0.01 mm/hour |
| Evaporative loss | Maximum of 100% of PET |

Table A-3: Parameter ranges for wetlands (State of NSW and Department of Planning and Environment, 2022b)

| Wetlands | Acceptable parameter ranges |
|--------------------------|--|
| Inlet pond volume | Set to zero if upstream sediment basin is modelled separately or sized to target 95% removal of 125 μ m particles for 4EY ¹ flow events |
| Extended detention depth | Maximum of 350 mm |
| Permanent pool volume | 0.3–0.4 m x wetland surface area |
| Exfiltration | Maximum of 0.01 mm/hour |
| Evaporative loss | Maximum of 125% of PET |
| Outlet pipe | Adjust to ensure notional detention time is within ranges |
| Notional detention time | 48–72 hours for detention depths of 100–350 mm No less than 48 hours for detention depths <100 mm |
| k & C* values (MUSIC) | Use default values |

1 4EY = 4 exceedances per year



Table A-4: Parameter ranges for bioretention (raingardens) (State of NSW andDepartment of Planning and Environment, 2022b)

| Bioretention | Acceptable parameter ranges |
|------------------------------------|---|
| Extended detention depth | Maximum of 300 mm |
| | Maximum of 150 mm in streetscape bioretention |
| Unlined filter media perimeter | 0.01 m (i.e. the systems are lined) |
| Saturate hydraulic conductivity | Maximum of 100 mm/hour |
| Filter media depth | 0.4–0.7 m |
| TN content | 800 mg/kg |
| Orthophosphate content | 40 mg/kg |
| Exfiltration rate | zero |
| Lining | Yes – base is lined |
| Underdrain present | Yes |
| k & C* values (MUSIC) | Use default values |

Table A-5: Parameter ranges for storage ponds (dams) (State of NSW and Departmentof Planning and Environment, 2022b)

| Storage ponds | Acceptable parameter ranges |
|-----------------------|---|
| Water source | Only roof water or treated water into reuse storage ponds |
| Surface area | User defined |
| Permanent pool volume | Calculate with depth up to a maximum of 3.0 m |
| Initial volume | Same as permanent pool volume |
| Exfiltration rate | Maximum of 0.01 mm/hour |
| Evaporative loss | Maximum of 100% of PET |
| Reuse demands | Irrigation to be modelled as an annual demand Distribution* to be defined with a monthly pattern which is (Jan–Dec): 13%, 6%, 6%, 4%, 2%, 0%, 4%, 7%, 12%, 14%, 13%, 19% Indoor reuse to be modelled as a daily demand |

* Irrigation distribution takes into account PET, rainfall and crop types



Appendix B MUSIC model details



Figure B-1: MUSIC model schematic - Sydney Water - Northwest cluster



Figure B-2: MUSIC model schematic – TWG Stormwater Consultant - Northwest cluster





Figure B-3: MUSIC model schematic - Sydney Water - East cluster



Figure B-4: MUSIC model schematic – TWG Stormwater Consultant - East cluster



B.2 MUSIC model inputs

B.2.1 Sydney Water Northwest Cluster

Table B-1: Source node information – Sydney Water - Northwest cluster

| | | | | | | Netland | Pond 2 + | | | | | | | | | | | | | | | NW01 | | NW03 |
|---|--------------|----------|-------------|---------------|------------|------------|------------|-----------|---------------|-----------|---------------|------------|-----------|--------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| | NW01 10 | | NW01 Lo | | | 2A + 2B | Pond 3 | Wetland | NW02 10 | | NW02 Lo | | | NW03 10 | | NW03 Lo | | | F06a PO | NorthWe | Wetland | bio 1 | NW02 | bio |
| | 0% Lot R M | W01 Lo | t Landsc | NW01 St | NW01 St | direct | direct | 4 direct | 0% Lot R | NW02 Lo | t Landsc | NW02 St | NW02 St | 0% Lot R | NW03 Lo | t Landsc | NW03 St | NW03 St | S Landsc | st POS L | 1 direct | direct | bio direct | direct |
| Location | oof t | Pave | ape | Pave | Perv | ainfall | rainfall | rainfall | oof | t Pave | ape | Pave | Perv | oof | t Pave | ape | Pave | Perv | ape | andscape | rainfall | rainfall | rainfall | rainfall |
| ID | 1 | - 2 | 2 3 | 3 4 | - 5 | 6 | 7 | | 9 | - 10 |) 11 | 12 | 13 | 3 14 | - 15 | . 16 | 17 | - 18 | . 19 | 20 | 21 | 50 | 51 | 52 |
| Node Type | UrbanSou L | JrbanSou | UrbanSou | u UrbanSou | UrbanSou | JrbanSou | UrbanSou | UrbanSo | u UrbanSou | UrbanSou | u UrbanSou | UrbanSou | UrbanSou | u UrbanSou | UrbanSour |
| Zoning Surface Type | Roof I | ndustria | I Industria | Sealedroa | Sealedroal | Revegetat | Revegeta | Revegeta | 1 Roof | Industria | Industrial | Sealedroa | Sealedro | a Roof | Industrial | Industrial | Sealedroa | Sealedroa | Revegetat | Revegetat | Revegetat | Revegeta | Revegetat | Revegetat |
| Total Area (ha) | 21.47 | 11.71 | 5.86 | 5 2.13 | 0.66 | 0.837 | 7.12 | 0.94 | 24.72 | 13.48 | 6.74 | 9.78 | 3 | 31.14 | 16.98 | 8.49 | 5.49 | 1.69 | 2.91 | 30.72 | 0.69 | 0.231 | 0.419 | 0.471 |
| Area Impervious (ha) | 21.47 | 11.71 | | 2.13 | 0 | 0.7533 | 6.408 | 0.847 | 3 24.72 | 13.48 | 3 0 | 9.78 | | 31.14 | 16.98 | 0 | 5.49 | 0 | 0 | 0 | 0.621 | 0 | 0 | 0 |
| Area Pervious (ha) | 0 | (| 5.86 | 5 0 | 0.66 | 0.0837 | 0.712 | 0.094 | 2 0 | (| 6.74 | 0 |) 3 | 3 0 | 0 | 8.49 | 0 | 1.69 | 2.91 | 30.72 | 0.069 | 0.231 | 0.419 | 0.471 |
| Field Capacity (mm) | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 13 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 |
| Pervious Area Infiltration Canacity coefficient - a | 175 | 179 | 179 | 5 175 | 175 | 175 | 175 | 17 | 175 | 179 | 5 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 |
| Pervious Area Infiltration Canacity exponent - h | 2.5 | 21 | 5 25 | 5 25 | 2.5 | 2.5 | 2.5 | 2 | 25 | 21 | 5 25 | 25 | 25 | 25 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| Impervious Area Bainfall Threshold (mm/day) | 1 | 2.13 | 1 1 | 1 1 | 1 | 1 | 1 | | 1 | 2.13 | 1 1 | 1 | 1 | 1 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Penvious Area Soil Storage Canacity (mm) | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 15 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 |
| Pervious Area Soil Initial Storage (% of Canacity) | 30 | 30 | 1 30 | 30 | 30 | 30 | 30 | 3 | 30 | 30 | 30 | 30 |) 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| Groundwater Initial Denth (mm) | 10 | 10 |) 1(| 10 | 10 | 10 | 10 | 1 |) 10 | 1(| 10 | 10 | 10 |) 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| Groundwater Daily Becharge Bate (%) | 25 | 21 | 5 25 | 5 25 | 25 | 25 | 25 | 2 | 5 25 | 21 | 5 25 | 25 | 20 | 5 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| Groundwater Daily Receilage Nate (%) | 1.4 | 1. | 1 1/ | 1 1 / | 1.4 | 1.4 | 1.0 | 1 | 1 14 | 1. | 1 1 / | 1 1 4 | 1 | 1 1 1 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Groundwater Daily Deen Scopage Pate (%) | 1.4 | 1.4 | 1.5 | 1.4 | 1.4 | 1.4 | 1.4 | 1. | 1.4 | 1.4 | 1.4 | 1.4 | . 1 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Stormflow Total Suspended Solids Mean (log mg/l.) | 1 2 | 2.43 | 2 2 10 | 2 2 4 2 | 2 / 2 | 1 05 | 1.05 | 10 | . 12 | 2.43 | 2 2 10 | 2/2 | 2/3 |) U | 2 / 2 | 2 15 | 2 / 2 | 2 / 2 | 1.05 | 1 05 | 1 05 | 1.05 | 1.05 | 1.05 |
| Stormflow Total Suspended Solids Standard Doviation (log mg/L) | 0.22 | 2.4 | 0 0 2.1. | 0 2.43 | 0.22 | 1.55 | 1.53 | 0.2 | 0 0 2 2 | 2.4 | 0 2.13 | 0 2.43 | 0 2.4. | 0 22 | 0.22 | 0.22 | 0.23 | 0.23 | 0.22 | 1.55 | 1.55 | 1.93 | 0.22 | 0.22 |
| Stormflow Total Suspended Solids Standard Deviation (log mg/ L) | Stochastic S | tochacti | Ctochasti | c Stochasti | Stochastic | tochastic | Stochasti | Stochasti | C Stochastic | Stochasti | C Stochasti | Stochastic | Stochasti | c Stochastic | Ctochastic | Stochastic |
| Stormflow Total Suspended Solids Estimation Method | Stochastic 3 | rounasu | | | 0 | | Stochastic | Stochasti | | Stochasti | | | | | Stochastic | otocnastic | Stochastic | otocnastic | o | otocnastic | o | Stochastic | o | o |
| Stormflow Total Descharus Mean (leg mg/l) | 0.90 | 0.7 | | . 03 | 0.2 | 0.66 | 0.66 | 0.6 | 0.00 | | | 0.2 | | | 0.2 | 0.6 | 0.2 | 0.2 | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 |
| Stormflow Total Phosphorus Standard Daviation (log mg/L) | -0.89 | -0.3 | -0.0 | -0.5 | -0.5 | -0.00 | -0.00 | -0.0 | -0.69 | -0.3 | -0.0 | -0.5 | -0.3 | -0.89 | -0.5 | -0.0 | -0.5 | -0.5 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 |
| Stormilow Total Phosphorus Standard Deviation (log mg/L) | 0.25 | 0.23 | 0.23 | 0.25 | 0.25 | 0.25 | 0.25 | 0.2 | 0.25 | 0.23 | 0.25 | 0.25 | 0.23 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| Stormflow Total Phosphorus Estimation Method | Stochastics | tocnasti | c stocnasti | c Stochastic | Stochastic | stochastic | Stochastic | Stochasti | c Stochastic | Stochasti | c Stochastic | stochastic | stocnasti | c Stochastic | stocnastic |
| Stormflow Total Phosphorus Serial Correlation | 0 | | | | 0 | 0 | 0 | | 0 | | | 0 | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Nitrogen Mean (log mg/L) | 0.3 | 0.34 | + 0.3 | 3 0.34 | 0.34 | 0.3 | 0.3 | 0.1 | 0.3 | 0.34 | + 0.3 | 0.34 | 0.34 | + U.3 | 0.34 | 0.3 | 0.34 | 0.34 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| Stormflow Total Nitrogen Standard Deviation (log mg/L) | 0.19 | 0.15 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.1 | 0.19 | 0.15 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Stormflow Total Nitrogen Estimation Method | Stochastics | tochasti | c Stochasti | c Stochastic | Stochastic | stochastic | Stochastic | Stochasti | c Stochastic | Stochasti | c Stochastic | Stochastic | Stochasti | c Stochastic | stochastic |
| Stormflow Total Nitrogen Serial Correlation | 0 | (| | 0 | 0 | 0 | 0 | (| 0 | (| 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Suspended Solids Mean (log mg/L) | 1.2 | 1.2 | 2 1.2 | 2 1.2 | 1.2 | 1.15 | 1.15 | 1.1 | 5 1.2 | 1.2 | 2 1.2 | 1.2 | 1.2 | 2 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 |
| Baseflow Total Suspended Solids Standard Deviation (log mg/L) | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.1 | 0.17 | 0.1 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Baseflow Total Suspended Solids Estimation Method | Stochastic S | tochasti | c Stochasti | c Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | c Stochastic | Stochasti | c Stochastic | Stochastic | Stochasti | c Stochastic | Stochastic |
| Baseflow Total Suspended Solids Serial Correlation | 0 | (|) (| 0 0 | 0 | 0 | 0 | (| 0 0 | (| 0 0 | 0 0 | C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Phosphorus Mean (log mg/L) | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -1.22 | -1.22 | -1.2 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 |
| Baseflow Total Phosphorus Standard Deviation (log mg/L) | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.1 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Baseflow Total Phosphorus Estimation Method | Stochastic S | tochasti | c Stochasti | c Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | c Stochastic | Stochasti | c Stochasti | Stochastic | Stochasti | c Stochastic | Stochastic |
| Baseflow Total Phosphorus Serial Correlation | 0 | (|) (| 0 0 | 0 | 0 | 0 | (| 0 0 | (| 0 0 | 0 |) C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Nitrogen Mean (log mg/L) | 0.11 | 0.11 | L 0.11 | L 0.11 | 0.11 | -0.05 | -0.05 | -0.0 | 5 0.11 | 0.11 | L 0.11 | 0.11 | 0.11 | l 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 |
| Baseflow Total Nitrogen Standard Deviation (log mg/L) | 0.12 | 0.12 | 2 0.12 | 2 0.12 | 0.12 | 0.12 | 0.12 | 0.1 | 2 0.12 | 0.12 | 2 0.12 | 0.12 | 0.12 | 2 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| Baseflow Total Nitrogen Estimation Method | Stochastic S | tochasti | c Stochasti | c Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic | Stochasti | c Stochasti | Stochastic | Stochasti | c Stochastic | Stochastic |
| Baseflow Total Nitrogen Serial Correlation | 0 | (| 0 0 | 0 0 | 0 | 0 | 0 | (| 0 0 | (| 0 0 | 0 | C C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Flow based constituent generation - enabled | Off C | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Dff |
| Flow based constituent generation - flow file | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - base flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - pervious flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - impervious flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - unit | | | | | | | | | | | | | | | | | | | | | | | | |



Table B-2: UTSM treatment nodes – Sydney Water - Northwest cluster

| | | | Wetland | | | | | NW01_Bi | NW02_Bi | Altis_Bio | Altis_Bio | |
|--|---------|----------|-----------|----------|------------|-----------|----------|-----------|-----------|-----------|-----------|----------|
| | Wetland | Wetland | 1 - up to | Pond 2 + | NW01_0 | NW02_0 | NW03_0 | oretentio | oretentio | retention | retention | |
| Location | 2A + 2B | 4 | 10322 | Pond 3 | p4_StTr | p4_StTr | p4_StTr | n | n | Sth | Nth | Pond 1 |
| | 22 | 23 | 24 | 25 | 26 | 2/ | 28 | 44 | 45 | 46 | 54 | 55 |
| Node Type | Wetland | WetlandN | Wetland | PondNod | BioRetent | BioRetent | BioReten | BioReten | BioRetent | BioReten | BioRetent | PondNode |
| LO-HOW Dypass rate (cum/sec) | 12 5 | 15 | 12 | 100 | 100.009 | 100 136 | 0.15 | 100 | 100 | 100 | 1 | 100 |
| Ini-itow bypass rate (cull/sec) | 1022.6 | 2070 | 2200.1 | 100 | 100.098 | 100.150 | 0.15 | 100 | 100 | 100 | 1 | 100 |
| Area (som) | 4333.0 | 9575 | 6920 | 6632/ | 653 | 901 | 996 | 6921 | /186 | 1/1286 | 1406 | 10323 |
| Initial Volume (m^3) | 2512 | 2708 | 2076 | 116408 | 000 | 501 | 550 | 0521 | 4100 | 14200 | 1400 | 18474 |
| Extended detention depth (m) | 0.05 | 0.05 | 0.3 | 0.05 | 0.02 | 0.02 | 0.02 | 0.3 | 0.3 | 0.3 | 0.3 | 0.05 |
| Number of Bainwater tanks | 0.05 | 0.05 | 0.5 | 0.05 | 0.02 | 0.02 | 0.02 | 0.5 | 0.5 | 0.5 | 0.5 | 0.05 |
| Permanent Pool Volume (cubic metres) | 2512 | 2708 | 2076 | 116408 | | | | | | | | 18474 |
| Proportion vegetated | 0.5 | 0.5 | 0.5 | 0.1 | | | | | | | | 0.1 |
| Equivalent Pipe Diameter (mm) | 68 | 73 | 97 | 171 | | | | | | | | 68 |
| Overflow weir width (m) | 5 | 5 | 5 | 20 | 2 | 2 | 2 | 20 | 8 | 20 | 8 | 20 |
| Notional Detention Time (hrs) | 48.3 | 47.9 | 48 | 60.5 | | | | | | | | 59.5 |
| Orifice Discharge Coefficient | 0.6 | 0.6 | 0.6 | 0.6 | | | | | | | | 0.6 |
| Weir Coefficient | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 |
| Number of CSTR Cells | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 2 |
| Total Suspended Solids - k (m/yr) | 1500 | 1500 | 1500 | 400 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 400 |
| Total Suspended Solids - C* (mg/L) | 6 | 6 | 6 | 12 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 12 |
| Total Suspended Solids - C** (mg/L) | 6 | 6 | 6 | 12 | | | | | | | | 12 |
| Total Phosphorus - k (m/yr) | 1000 | 1000 | 1000 | 300 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 300 |
| Total Phosphorus - C* (mg/L) | 0.06 | 0.06 | 0.06 | 0.09 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.09 |
| Total Phosphorus - C** (mg/L) | 0.06 | 0.06 | 0.06 | 0.09 | | | | | | | | 0.09 |
| Total Nitrogen - k (m/yr) | 150 | 150 | 150 | 40 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 40 |
| Total Nitrogen - C* (mg/L) | 1 | 1 | 1 | 1 | . 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1 |
| Throshold Hydraulic Loading for C** (m/ur) | 2500 | 2500 | 2500 | . 1 | | | | | | | | 2500 |
| Horizontal Flow Coefficient | 3500 | 3500 | 3500 | , 3500 | , | - | - | - | - | - | - | 3500 |
| Reuse Enabled | Off | Off | Off | On | 3 Off | 3 Off | Off 3 | Off 3 | 3 Off | Off 3 | 3 Off | On |
| Max drawdown hoight (m) | UII | UII | 011 | 1 755 | | 011 | UII | UII | 011 | 011 | 011 | 1 700002 |
| Annual Demand Enabled | Off | Off | Off | 0n | Off | Off | Off | Off | Off | Off | Off | 0n |
| Annual Demand Value (MI /vear) | UII | UII | 011 | 95 37 | , | UII | UII | UII | UII | 011 | 011 | 35 11 |
| Annual Demand Distribution | | | | Monthly | | | | | | | | Monthly |
| Annual Demand Monthly Distribution: Jan | | | | 13 | | | | | | | | 13 |
| Annual Demand Monthly Distribution: Eeb | | | | | | | | | | | | |
| Annual Demand Monthly Distribution: Mar | | | | 6 | | | | | | | | 6 |
| Annual Demand Monthly Distribution: Apr | | | | 4 | | | | | | | | 4 |
| Annual Demand Monthly Distribution: May | | | | 2 | | | | | | | | 2 |
| Annual Demand Monthly Distribution: Jun | | | | C | | | | | | | | 0 |
| Annual Demand Monthly Distribution: Jul | | | | 4 | | | | | | | | 4 |
| Annual Demand Monthly Distribution: Aug | | | | 7 | | | | | | | | 7 |
| Annual Demand Monthly Distribution: Sep | | | | 12 | | | | | | | | 12 |
| Annual Demand Monthly Distribution: Oct | | | | 14 | | | | | | | | 14 |
| Annual Demand Monthly Distribution: Nov | | | | 13 | | | | | | | | 13 |
| Annual Demand Monthly Distribution: Dec | | | | 19 |) | | | | | | | 19 |
| Daily Demand Enabled | Off | Off | Off | On | Off | Off | Off | Off | Off | Off | Off | On |
| Daily Demand Value (ML/day) | | | | 0.474 | | | | | | | | 0.174 |
| Custom Demand Enabled | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Custom Demand Time Series File | | | | | | | | | | | | |
| Custom Demand Time Series Units | | | | | | | | | | | | |
| Filter area (sqm) | | | | | 653 | 901 | 996 | 2307 | 4186 | 4709 | 1406 | |
| Filter perimeter (m) | | | | | 0.01 | 0.01 | 0.01 | . 14 | 14 | 14 | 14 | |
| Filter depth (m) | | | | | 0.52 | 0.52 | 0.52 | 0.5 | 0.5 | 0.5 | 0.5 | |
| Filter Median Particle Diameter (mm) | | | | | | | | | | | | |
| Saturated Hydraulic Conductivity (mm/hr) | | | | | 25 | 25 | 25 | 100 | 100 | 100 | 100 | |
| Infiltration Media Porosity | | | | | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | |
| Length (m) | | | | | | | | | | | | |
| Paso Width (m) | | | | | | | | | | | | |
| Top width (m) | | | | | | | | | | | | |
| Vegetation height (m) | | | | | | | | | | | | |
| Vegetation Type | | | | | Vegetator | Vegetator | Vegetata | Vegetata | Vegetator | Vegetato | Vegetator | |
| Total Nitrogen Content in Filter (mg/kg) | | | | | * cgetated | 100 | Ann | AUD | 100 | 100 | 100 | |
| Orthonhosphate Content in Filter (mg/kg) | | | | | 400 | 400 | 400 | 400 | 400 | 400 | 400 | |
| Is Base Lined? | | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Is Underdrain Present? | | | | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Is Submerged Zone Present? | | | | | No | No | No | No | No | No | No | |
| Submerged Zone Depth (m) | | | | | | | | | | | | |
| B for Media Soil Texture | -9999 | -9999 | -9999 | -9999 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | -9999 |
| Proportion of upstream impervious area treated | | | | | | | | | | | | |
| Exfiltration Rate (mm/hr) | 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Evaporative Loss as % of PET | 125 | 125 | 125 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Depth in metres below the drain pipe | | | | | | | | | | | | |
| TSS A Coefficient | | | | | | | | | | | | |
| TSS B Coefficient | | | | | | | | | | | | |
| TP A Coefficient | | | | | | | | | | | | |
| TP B Coefficient | | | | | | | | | | | | |
| TN A Coefficient | | | | | | | | | | | | |
| TN B Coefficient | | | | | | | | | | | | |
| Sfc | | | | | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | |
| S* | - | | | | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | |
| Sw | | | | | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | |
| Sh | | | | | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | |
| Emax (m/day) | | | | | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | |
| Ew (m/day) | | | | | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | |



Table B-3: Generic treatment nodes - Sydney Water - Northwest cluster

| | | | | | | | | 1 | | |
|--|---------|---------|---------|---------|---------|---------|-------------|-------------|-------------|-------------|
| | | | | | | | Generic | Generic | Generic | |
| | | | | | | | Treatme | Treatme | Treatme | Generic |
| | NW01_Lo | NW01_E | NW02_Lo | NW02_E | NW03_Lo | NW03_E | nt Node | nt Node | nt Node | Treatme |
| Location | t_GPT | OP_GPT | t_GPT | OP_GPT | t_GPT | OP_GPT | 2.70000 | 3.33000 | 3.60000 | nt Node |
| ID | 38 | 39 | 40 | 41 | 42 | 43 | 47 | 48 | 49 | 53 |
| Node Type | GPTNode | GPTNode | GPTNode | GPTNode | GPTNode | GPTNode | GenericN | GenericNo | GenericN | GenericNo |
| Lo-flow bypass rate (cum/sec) | C | 99 | 0 | 99 | 0 | 99 | 0 | 0 | 0 | 0.0125 |
| Hi-flow bypass rate (cum/sec) | 0.66 | 5 100 | 0.76 | 100 | 0.96 | 100 | 2.7 | 3.33 | 15 | 100 |
| Flow Transfer Function | | | | | | | | | | |
| Input (cum/sec) | C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Output (cum/sec) | C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Input (cum/sec) | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 20 |
| Output (cum/sec) | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 20 |
| Gross Pollutant Transfer Function | | | | | | | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (kg/ML) | C | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Output (kg/ML) | C | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Input (kg/ML) | 100 | 100 | 100 | 100 | 100 | 100 | 15 | 15 | 15 | 15 |
| Output (kg/ML) | 2 | 2 2 | 2 | 2 | 2 | 2 | 15 | 15 | 15 | 15 |
| Total Nitrogen Transfer Function | | | | | | | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | C | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 |
| Output (mg/L) | C | 0 | C | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 |
| Input (mg/L) | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| Output (mg/L) | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| Total Phosphorus Transfer Function | | | | | | | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | (| 0 0 | C | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 |
| Output (mg/L) | (| 0 0 | C | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 |
| Input (mg/L) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 5 | 5 | 5 | 5 |
| Output (mg/L) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 5 | 5 | 5 | 5 |
| Input (mg/L) | 10 | 10 | 10 | 10 | 10 | 10 | | | | |
| Output (mg/L) | 7 | 7 | 7 | 7 | 7 | 7 | , | | | - |
| Total Suspended Solids Transfer Function | | | | | | | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | (| 0 0 | C |) C | 0 | C | 0 | 0 0 | 0 | 0 0 |
| Output (mg/L) | (| 0 0 |) C |) C | 0 | C | 0 | 0 0 | 0 | 0 0 |
| Input (mg/L) | 75 | 5 75 | 75 | 75 | 75 | 75 | 1000 | 1000 | 1000 | 1000 |
| Output (mg/L) | 75 | 5 75 | 75 | 75 | 75 | 75 | 1000 | 1000 | 1000 | 1000 |
| Input (mg/L) | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 |) | | | |
| Output (mg/L) | 300 | 300 | 300 | 300 | 300 | 300 |) | | | |
| TSS Flow based Efficiency Enabled | Off | Off | Off | Off | Off | Off | On | On | On | On |
| TSS Flow based Efficiency | | | | | | | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] |
| TP Flow based Efficiency Enabled | Off | Off | Off | Off | Off | Off | On | On | On | On |
| TP Flow based Efficiency | | | | | | | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] |
| TN Flow based Efficiency Enabled | Off | Off | Off | Off | Off | Off | On | On | On | On |
| TN Flow based Efficiency | | | | | | | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] |
| GP Flow based Efficiency Enabled | Off | Off | Off | Off | Off | Off | On | On | On | On |
| GP Flow based Efficiency | | | | | | | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] | [0:1];[1:1] |

Table B-4: Other nodes - Sydney Water - Northwest cluster

| | | NW01_Tr | | | NW02_Tr | | NW03_Tr | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | NW01_L | unk | South | NW02_L | unk | NW03_L | unk | Wetland | |
| Location | OT_Jnc | drainage | Creek | OT_Jnc | drainage | OT_Jnc | drainage | Pond 2+3 | Junction |
| ID | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 |
| Node Type | JunctionN |



B.2.2 TWG stormwater consultant Northwest Cluster Alternative 1

Table B-5: Source node information – TWG stormwater consultant - Northwest cluster

| | | | | | Pond | 2 + | | | | | | | | | | | | | | NW03 | Addition | | Addition | |
|--|------------|------------|------------|------------|------------------|---------------|------------|--------------|--------------|-------------|------------|-----------|-------------|--------------|------------|------------|-----------|-------------|------------|------------|--------------|-----------|-----------|---------------|
| | NW01_10 | | NW01_Lo | | Pond | 3 Wetlan | I NW02_: | 0 | NW02_Lo | | | NW03_10 |) | NW03_Lo | | | F06a_PO | NorthWe | WSUD | bio | al | WSUD | al | WSDUD |
| | 0%_Lot_R | NW01_Lo | t_Landsc | NW01_St | NW01_St direc | 4 direct | 0%_Lot | R NW02_L | t_Landsc | NW02_St | NW02_St | 0%_Lot_R | NW03_Lo | t_Landsc | NW03_St | NW03_St | S_Landsc | st_POS_L | direct | direct | Landscap | direct | Landscap | Direct |
| Location | oof | t_Pave | ape | _Pave | _Perv rainfa | ll rainfall | oof | t_Pave | ape | _Pave | _Perv | oof | t_Pave | ape | _Pave | _Perv | ape | andscape | rainfall | rainfall | e - 2-3 | rainfall | e -1 | rainfall |
| ID | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 10 |) 11 | . 12 | 13 | 3 14 | 15 | 16 | 17 | 18 | 19 | 39 | 40 | 43 | 46 | 47 | / 49 |
| Node Type | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou Urba | Sou UrbanSo | u UrbanSo | u UrbanSo | u UrbanSou | UrbanSou | UrbanSou | UrbanSou | u UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | J UrbanSour |
| Zoning Surface Type | Roof | Industrial | Industrial | Sealedroa | Sealedroa Reve | getal Revege | at Roof | Industria | l Industrial | Sealedroa | Sealedroa | Roof | Industria | Industrial | Sealedroa | Sealedroa | Revegeta | 1 Revegetat | Revegetat | Revegeta | Revegeta | Revegeta | Revegeta | It Revegetat |
| Total Area (ha) | 21.47 | 11.71 | 5.86 | 2.13 | 0.66 | 5.5 0.9 | 2 24. | 72 13.4 | 8 6.74 | 9.78 | 3 | 31.14 | 16.98 | 8.49 | 5.49 | 1.69 | 2.91 | 30.72 | 0.419 | 0.25 | 2.85 | 0.14 | 0.55 | ó 0.1 |
| Area Impervious (ha) | 21.47 | 11.71 | . 0 | 2.13 | 0 | 4.95 0.84 | 8 24. | 72 13.4 | 8 C | 9.78 | 0 | 31.14 | 16.98 | 0 | 5.49 | 0 | C | 0 | 0 | 0 | 0 | (| (| J 0.09 |
| Area Pervious (ha) | 0 | 0 | 5.86 | 0 | 0.66 | 0.55 0.09 | 12 | 0 | 0 6.74 | L 0 | 3 | (C | 0 0 | 8.49 | 0 | 1.69 | 2.91 | 30.72 | 0.419 | 0.25 | 2.85 | 0.14 | 0.55 | 0.01 ز |
| Field Capacity (mm) | 130 | 130 | 130 | 130 | 130 | 130 1 | 0 1 | 30 13 | 0 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | J 130 |
| Pervious Area Infiltration Capacity coefficient - a | 175 | 175 | 175 | 175 | 175 | 175 1 | '5 1 | 75 17 | 5 175 | 5 175 | 175 | 175 | 5 175 | 5 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 ز |
| Pervious Area Infiltration Capacity exponent - b | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 2 | .5 2 | .5 2. | 5 2.5 | 5 2.5 | 2.5 | 2.5 | 5 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | i 2.5 |
| Impervious Area Rainfall Threshold (mm/day) | 1 | 1 | . 1 | . 1 | 1 | 1 | 1 | 1 | 1 1 | . 1 | . 1 | . 1 | L 1 | . 1 | 1 | 1 | 1 | . 1 | 1 | 1 | . 2.5 | 1 | 2.5 | 1 ذ |
| Pervious Area Soil Storage Capacity (mm) | 150 | 150 | 150 | 150 | 150 | 150 1 | 60 1 | 50 15 | 0 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | J 150 |
| Pervious Area Soil Initial Storage (% of Capacity) | 30 | 30 |) 30 | 30 | 30 | 30 | 30 | 30 3 | 0 30 |) 30 | 30 |) 30 | 30 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | y 30 | 30 | 30 | J 30 |
| Groundwater Initial Depth (mm) | 10 | 10 |) 10 | 10 | 10 | 10 | LÖ | 10 1 | 0 10 |) 10 |) 10 |) 10 | 0 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | J 10 |
| Groundwater Daily Recharge Rate (%) | 25 | 25 | 5 25 | 25 | 25 | 25 | 25 | 25 2 | 5 25 | 5 25 | 5 25 | 5 25 | 5 25 | 5 25 | 25 | 25 | 25 | 25 | 25 | 25 | , 25 | 25 | 25 | i 25 |
| Groundwater Daily Baseflow Rate (%) | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 1 | .4 1 | .4 1. | 4 1.4 | 1 1.4 | 1.4 | 1.4 | 4 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 4 1.4 |
| Groundwater Daily Deep Seepage Rate (%) | 0 | C | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 C |) (| 0 0 |) (|) (| 0 0 | 0 | 0 | (| 0 0 | 0 | C | J 0 |) (|) (| J 0 |
| Stormflow Total Suspended Solids Mean (log mg/L) | 1.3 | 2.43 | 2.15 | 2.43 | 2.43 | 1.95 1. | 95 1 | .3 2.4 | 3 2.15 | 5 2.43 | 2.43 | 3 1.3 | 3 2.43 | 3 2.15 | 2.43 | 2.43 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.9 | 1.9 | <i>i</i> 1.95 |
| Stormflow Total Suspended Solids Standard Deviation (log mg/L) | 0.32 | 0.32 | 2 0.32 | 0.32 | 0.32 | 0.32 0. | 32 0. | 32 0.3 | 2 0.32 | 2 0.32 | 0.32 | 2 0.32 | 2 0.32 | 2 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.3 | 0.3 | 2 0.32 |
| Stormflow Total Suspended Solids Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic |
| Stormflow Total Suspended Solids Serial Correlation | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) C |) (| 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) O |
| Stormflow Total Phosphorus Mean (log mg/L) | -0.89 | -0.3 | -0.6 | -0.3 | -0.3 | 0.66 -0. | -0. | 39 -0. | 3 -0.6 | -0.3 | -0.3 | -0.89 | -0.3 | -0.6 | -0.3 | -0.3 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | o -0.66 |
| Stormflow Total Phosphorus Standard Deviation (log mg/L) | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 0. | 25 0. | 25 0.2 | 5 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 ز |
| Stormflow Total Phosphorus Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic |
| Stormflow Total Phosphorus Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) (| 0 0 | 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) O |
| Stormflow Total Nitrogen Mean (log mg/L) | 0.3 | 0.34 | 0.3 | 0.34 | 0.34 | 0.3 0 | .3 0 | .3 0.3 | 4 0.3 | 0.34 | 0.34 | 0.3 | 3 0.34 | 0.3 | 0.34 | 0.34 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 3 0.3 |
| Stormflow Total Nitrogen Standard Deviation (log mg/L) | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 0. | .9 0. | 19 0.1 | 9 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |) 0.19 |
| Stormflow Total Nitrogen Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic |
| Stormflow Total Nitrogen Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) C | 0 0 | 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) 0 |
| Baseflow Total Suspended Solids Mean (log mg/L) | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.15 1. | .5 1 | .2 1. | 2 1.2 | 1.2 | 1.2 | 1.2 | 2 1.2 | 1.2 | 1.2 | 1.2 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | i 1.15 |
| Baseflow Total Suspended Solids Standard Deviation (log mg/L) | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 0. | .7 0. | L7 0.1 | 7 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | / 0.17 |
| Baseflow Total Suspended Solids Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic |
| Baseflow Total Suspended Solids Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) C | 0 0 | 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) 0 |
| Baseflow Total Phosphorus Mean (log mg/L) | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | 1.22 -1. | 2 -0. | 35 -0.8 | 5 -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | 2 -1.22 |
| Baseflow Total Phosphorus Standard Deviation (log mg/L) | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 0. | .9 0. | 19 0.1 | 9 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |) 0.19 |
| Baseflow Total Phosphorus Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | c Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | . Stochastic | Stochasti | Stochasti | c Stochastic |
| Baseflow Total Phosphorus Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) C | 0 0 | 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) 0 |
| Baseflow Total Nitrogen Mean (log mg/L) | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.05 -0. | 05 0. | l1 0.1 | 1 0.11 | 0.11 | 0.11 | 0.11 | l 0.11 | 0.11 | 0.11 | 0.11 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | i -0.05 |
| Baseflow Total Nitrogen Standard Deviation (log mg/L) | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 0. | .2 0. | L2 0.1 | 2 0.12 | 0.12 | 0.12 | 0.12 | 2 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 2 0.12 |
| Baseflow Total Nitrogen Estimation Method | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic Stoch | astic Stochas | ic Stochas | tic Stochast | c Stochasti | c Stochasti | Stochastic | Stochasti | c Stochasti | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochasti | c Stochastic |
| Baseflow Total Nitrogen Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 |) C | 0 0 | 0 0 | 0 | 0 | C | 0 | 0 | 0 | 0 | (| (|) 0 |
| Flow based constituent generation - enabled | Off | Off | Off | Off | Off Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Flow based constituent generation - flow file | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - base flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - pervious flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - impervious flow column | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - unit | | | | | | | | | | | | | | | | | | | | | | | | |



Table B-6: UTSM treatment nodes – TWG stormwater consultant - Northwest cluster

| | | | | | | | | | | Copy of | |
|--|----------|---------|------------|------------|------------|------------|------------|------------|------------|----------|----------|
| | Wetland | Pond 2+ | NW01_0 | NW02 O | NW03 O | NW02_Bi | Altis_Bio | Altis_Bio | Sedimen | Sedimen | Sedimen |
| location | 4 | Pond 3 | p4 StTr | p4_StTr | p4 StTr | n | Sth | Nth | Basin | Basin | Basin |
| ID | 20 | 21 | 22 | 23 | 24 | 37 | 38 | 42 | 44 | 45 | 48 |
| Node Type | WetlandN | PondNod | BioRetent | BioReten | BioReten | t BioReten | BioRetent | BioReten | t Sediment | Sediment | Sediment |
| Lo-flow bypass rate (cum/sec) | 0 | 0 | 99 | 99 | 0.15 | 0 0 | 0 | 0 | 0 | 0 | 0 |
| Inlet nond volume | 15 | 100 | 100.098 | 100.150 | 0.15 | 100 | 100 | 1 | 100 | 001 | 100 |
| Area (sgm) | 9575 | 55000 | 653 | 901 | 996 | 4000 | 13075 | 1406 | 500 | 400 | 1000 |
| Initial Volume (m^3) | 2872.5 | 165000 | | | | | | | 500 | 400 | 1500 |
| Extended detention depth (m) | 0.05 | 0.08 | 0.02 | 0.02 | 0.02 | 0.3 | 0.3 | 0.3 | 0.01 | 0.01 | 0.01 |
| Number of Rainwater tanks | 2072 5 | 465000 | | | | | | | 500 | | 4500 |
| Proportion vegetated | 28/2.5 | 165000 | | | | | | | 500 | 400 | 1500 |
| Equivalent Pipe Diameter (mm) | 73 | 171 | | | | | | | 1000 | 1000 | 1000 |
| Overflow weir width (m) | 5 | 20 | 2 | 2 | 2 | . 8 | 20 | 8 | 10 | 10 | 10 |
| Notional Detention Time (hrs) | 47.9 | 63.4 | | | | | | | 5.96E-03 | 4.77E-03 | 1.19E-02 |
| Orifice Discharge Coefficient | 0.6 | 0.6 | | | | | | | 0.6 | 0.6 | 0.6 |
| Weir Coefficient | 1.7 | 1./ | 1.7 | 1./ | 1./ | 1.7 | 1.7 | 1./ | 1.7 | 1./ | 1.7 |
| Total Suspended Solids - k (m/vr) | 1500 | 400 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 |
| Total Suspended Solids - C* (mg/L) | 6 | 12 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| Total Suspended Solids - C** (mg/L) | 6 | 12 | | | | | | | 20 | 20 | 20 |
| Total Phosphorus - k (m/yr) | 1000 | 300 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 |
| Total Phosphorus - C* (mg/L) | 0.06 | 0.09 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Total Nitrogen - k (m/vr) | 150 | 40 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 |
| Total Nitrogen - C* (mg/L) | 1 | 1 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Total Nitrogen - C** (mg/L) | 1 | 1 | | | | | | | 1.4 | 1.4 | 1.4 |
| Threshold Hydraulic Loading for C** (m/yr) | 3500 | 3500 | | | | | | | 3500 | 3500 | 3500 |
| Horizontal Flow Coefficient | Off | 02 | 3 | 3 Off | 3 Off | 3 3 Off | 3 | Off 3 | Off | Off | Off |
| Max drawdown height (m) | UII | 2 990 | UII | UII | UII |
| Annual Demand Enabled | Off | On | Off | Off | Off |
| Annual Demand Value (ML/year) | | 140.68 | | | | | | | | | |
| Annual Demand Distribution | | Monthly | | | | | | | | | |
| Annual Demand Monthly Distribution: Jan | | 13 | | | | | | | | | |
| Annual Demand Monthly Distribution: Feb | | 6 | | | | | | | | | |
| Annual Demand Monthly Distribution: Mar | | 4 | | | | | | | | | |
| Annual Demand Monthly Distribution: May | | 2 | | | | | | | | | |
| Annual Demand Monthly Distribution: Jun | | 0 | | | | | | | | | |
| Annual Demand Monthly Distribution: Jul | | 4 | | | | | | | | | |
| Annual Demand Monthly Distribution: Aug | | 7 | | | | | | | | | |
| Annual Demand Monthly Distribution: Sep | | 12 | | | | | | | | | |
| Annual Demand Monthly Distribution: Nov | | 13 | | | | | | | | | |
| Annual Demand Monthly Distribution: Dec | | 19 | | | | | | | | | |
| Daily Demand Enabled | Off | On | Off | Off | Off |
| Daily Demand Value (ML/day) | Off | 0.648 | Off | Off | off | Off | off | 0# | Off | Off | off |
| Custom Demand Time Series File | UII | UII | UII | UII | UII | Uff | UII | Un | Un | UII | UIT |
| Custom Demand Time Series Units | | | | | | | | | | | |
| Filter area (sqm) | | | 653 | 901 | 996 | 3500 | 2500 | 1006 | i | | |
| Filter perimeter (m) | | | 0.01 | 0.01 | 0.01 | 0.01 | 14 | - 14 | | | |
| Filter depth (m) | | | 0.52 | 0.52 | 0.52 | 2 0.5 | 0.5 | 0.5 | | | |
| Saturated Hydraulic Conductivity (mm/hr) | | | 25 | 25 | 25 | 5 100 | 100 | 100 | 1 | | |
| Infiltration Media Porosity | | | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | i | | |
| Length (m) | | | | | | | | | | | |
| Bed slope | | | | | | | | | | | |
| Base Width (m) | | | | | | | | | | | |
| Vegetation height (m) | | | | | | | | | | | |
| Vegetation Type | | | Vegetate | Vegetate | Vegetate | Vegetate | Vegetate | Vegetate | ¢ | | |
| Total Nitrogen Content in Filter (mg/kg) | | | 400 | 400 | 400 | 400 | 400 | 400 | | | |
| Orthophosphate Content in Filter (mg/kg) | | | 40 | 40 | 40 | 40 | 40 | 40 | | | |
| Is base Lined? | | | Yes Ves | res Vos | Yes Ves | Yes | Yes Ves | res Ves | | | |
| Is Submerged Zone Present? | | | No | No | No | No | No | No | | | |
| Submerged Zone Depth (m) | | | | | | | | | | | |
| B for Media Soil Texture | -9999 | -9999 | 13 | 13 | 13 | 13 | 13 | 13 | -9999 | -9999 | -9999 |
| Proportion of upstream impervious area treated | | | | | | | | | | | |
| Extilitration Rate (mm/hr) | 0 | 100 | 0 | 100 | 100 | 0 0 | 0 | 100 | 0 | 0 | 0 |
| Depth in metres below the drain pine | 125 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | /5 | /5 | /5 |
| TSS A Coefficient | | | | | | | | | | | |
| TSS B Coefficient | | | | | | | | | | | |
| TP A Coefficient | | | | | | | | | | | |
| TP B Coefficient | | | | | | | | | | | |
| IN A COEfficient | | | | | | | | | | | |
| Sfc | | | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | | | |
| S* | | | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | | | |
| Sw | | | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | | | |
| Sh | | | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | | | |
| Emax (m/day) | | | 0.008 | 0.008 | 0.008 | 0.001 | 0.008 | 0.001 | 1 | | |
| (, uuy) | | I | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 1 | | |

Sydney Aerotropolis - Mamre Road MUSIC Model Review



| | | | | Generic |
|--|---------|---------|---------|-------------|
| | NW01_Lo | NW02_Lo | NW03_Lo | Treatme |
| Location | t_GPT | t_GPT | t_GPT | nt Node |
| ID | 34 | 35 | 36 | 41 |
| Node Type | GPTNode | GPTNode | GPTNode | GenericN |
| Lo-flow bypass rate (cum/sec) | 0 | 0 | 0 | 0.0125 |
| Hi-flow bypass rate (cum/sec) | 0.66 | 0.76 | 0.96 | 100 |
| Flow Transfer Function | | | | |
| Input (cum/sec) | 0 | 0 | 0 | 0 |
| Output (cum/sec) | 0 | 0 | 0 | 0 |
| Input (cum/sec) | 10 | 10 | 10 | 20 |
| Output (cum/sec) | 10 | 10 | 10 | 20 |
| Gross Pollutant Transfer Function | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (kg/ML) | 0 | 0 | 0 | 0 |
| Output (kg/ML) | 0 | 0 | 0 | 0 |
| Input (kg/ML) | 100 | 100 | 100 | 15 |
| Output (kg/ML) | 2 | 2 | 2 | 15 |
| Total Nitrogen Transfer Function | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 | 0 |
| Input (mg/L) | 50 | 50 | 50 | 50 |
| Output (mg/L) | 50 | 50 | 50 | 50 |
| Total Phosphorus Transfer Function | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 | 0 |
| Input (mg/L) | 0.5 | 0.5 | 0.5 | 5 |
| Output (mg/L) | 0.5 | 0.5 | 0.5 | 5 |
| Input (mg/L) | 10 | 10 | 10 | |
| Output (mg/L) | 7 | 7 | 7 | |
| Total Suspended Solids Transfer Function | | | | |
| Enabled | TRUE | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 | 0 |
| Input (mg/L) | 75 | 75 | 75 | 1000 |
| Output (mg/L) | 75 | 75 | 75 | 1000 |
| Input (mg/L) | 1000 | 1000 | 1000 | |
| Output (mg/L) | 300 | 300 | 300 | |
| TSS Flow based Efficiency Enabled | Off | Off | Off | On |
| TSS Flow based Efficiency | | | | [0:1]:[1:1] |
| TP Flow based Efficiency Enabled | Off | Off | Off | On |
| TP Flow based Efficiency | | | | [0:1]:[1:1] |
| TN Flow based Efficiency Enabled | Off | Off | Off | On |
| TN Flow based Efficiency | | 5.1 | | [0:1]·[1·1] |
| GP Flow based Efficiency Enabled | Off | Off | Off | On |
| GP Flow based Efficiency | | | | [0·1]·[1·1] |
| Si from Subcu Efficiency | | | | [[]]]] |

Table B-7: Generic treatment nodes – TWG stormwater consultant - Northwest cluster



Table B-8: Other nodes – TWG stormwater consultant - Northwest cluster

| | | NW01_Tr | | | NW02_Tr | | NW03_Tr | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | NW01_L | unk | South | NW02_L | unk | NW03_L | unk | Wetland | | |
| Location | OT_Jnc | drainage | Creek | OT_Jnc | drainage | OT_Jnc | drainage | Pond 2+3 | Junction | Junction |
| ID | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 50 |
| Node Type | JunctionN |



B.2.3 Sydney Water East Cluster

Table B-9: Source node information – Sydney Water - East cluster

| Source nodes | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|-----------|---------------|------------|------------|------------|------------|---------------|------------|------------|---------------|---------------|-------------|-----------|-----------------|-----------------|-----------|------------|----------------|---------------|-----------|--------------|--------------|-----------|------------|------------|------------|
| | | | | | | Wetland | | | | | | | | | | | | | | | | P | ond | | | Bio |
| | | Wetland | Pond 25 | Wetland | Pond 28 | 29+30+31 | E03_100 | | E03_Lot_ | | | E01_100 | | E01_Lot_ | | | E02_100 | | E02_Lot_ | | | 2 | 9+30+31 | Bio 25 | Bio 28 | 29+30+31 |
| | E01_int_ | 25 direct | direct | 28 direct | direct | direct | %_Lot_R E0 | 03_Lot_ | Landscap | E03_St_P | E03_St_P | %_Lot_R | E01_Lot_ | Landscap | 01_St_P | E01_St_P | %_Lot_R | E02_Lot_ | Landscap | E02_St_P | 5.180_St_ | E_ext_PO d | irect | direct | direct | direct |
| Location | POS | rainfall | rainfall | rainfall | rainfall | rainfall | oof Pa | ave e | e | ave | erv | oof | Pave | e a | ave | erv | oof | Pave | e | ave | Perv | S r | ainfall | rainfall | rainfall | rainfall |
| ID | | 1 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 9 10 |) 11 | L 12 | 13 | 3 14 | 15 | 16 | 17 | 18 | 19 | 20 |) 21 | 22 | 23 | 49 | 51 | 53 |
| Node Type | UrbanSo | u UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou | UrbanSou U | rbanSou I | UrbanSou | u UrbanSou | u UrbanSou | u UrbanSou | UrbanSou | u UrbanSou I | JrbanSou | UrbanSou | UrbanSou | UrbanSou | u UrbanSou | UrbanSou | u UrbanSou | UrbanSou L | IrbanSou | UrbanSou | UrbanSou | UrbanSour |
| Zoning Surface Type | Revegeta | al Revegetat | Revegetat | Revegetat | Revegetat | Revegetat | Roof In | dustrial I | Industrial | Sealedro | aSealedro | a Roof | Industria | Industrial S | Sealedroa | Sealedroa | Roof | Industria | Industrial | Sealedro | a Sealedroa | Revegetat F | evegetat | Revegetat | Revegeta | Revegetat |
| Total Area (ha) | 10.2 | 3 0.69 | 1.606 | 0.246 | 0.542 | 2.289 | 59.46 | 32.44 | 16.22 | 5.33 | 3 1.64 | 1 14.75 | 8.05 | 5 4.02 | 3.85 | 1.18 | 8.16 | 4.45 | 2.23 | 0.81 | L 0.25 | 51.62 | 4.997 | 0.246 | 0.088 | 0.817 |
| Area Impervious (ha) | | 0 0.621 | 1.4454 | 0.2214 | 0.4878 | 0.921408 | 59.46 | 32.44 | 0 | 5.33 | 3 (|) 14.75 | 8.05 | 5 0 | 3.85 | C | 8.16 | 4.45 | 6 0 | 0.81 | L 0 | 0 | 4.997 | 0 | 0 | 0 |
| Area Pervious (ha) | 10.2 | 3 0.069 | 0.1606 | 0.0246 | 0.0542 | 1.367592 | 0 | 0 | 16.22 | 2 (| 1.64 | 1 C |) (| 4.02 | 0 | 1.18 | 0 | (| 2.23 | (| 0.25 | 51.62 | 0 | 0.246 | 0.088 | 0.817 |
| Field Capacity (mm) | 13 | 0 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 |) 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 |
| Pervious Area Infiltration Capacity coefficient - a | 17 | 5 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 5 175 | 5 175 | 5 175 | 175 | 5 175 | 175 | 175 | 175 | 175 | 175 | 175 | 5 175 | 175 | 175 | 175 | 175 | 175 |
| Pervious Area Infiltration Capacity exponent - b | 2. | 5 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 5 2.5 | 5 2.5 | 2.5 | 5 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 5 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| Impervious Area Rainfall Threshold (mm/day) | | 1 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 1 | 1 1 | 1 | 1 1 | 1 | 1 | 1 | 1 | 1 | | 1 1 | 1 | 1 | 1 | 1 | 1 |
| Pervious Area Soil Storage Capacity (mm) | 15 | 0 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 |) 150 |) 150 | 150 | 150 | 0 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 |
| Pervious Area Soil Initial Storage (% of Capacity) | 3 | 0 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |) 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| Groundwater Initial Depth (mm) | 1 | 0 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |) 10 | 0 10 | 0 10 |) 10 | 0 10 | 10 | 10 | 0 10 | 10 |) 10 | 10 | 0 10 | 10 | 10 | 10 | 10 | 10 |
| Groundwater Daily Recharge Rate (%) | 2 | 5 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 5 2 | 5 24 | 5 29 | 2 | 5 25 | 25 | 25 | 25 | 24 | 5 25 | 2 | 5 25 | 25 | 25 | 25 | 25 | 25 |
| Groundwater Daily Baseflow Rate (%) | 1 | 4 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1 1.4 | 4 1.4 | 4 1.4 | 1 1.4 | 4 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1 1.4 | 1.4 | 4 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Groundwater Daily Deen Seenage Rate (%) | | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | n (|) (| n 0 | | |) () | | 1 0 | | n 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Suspended Solids Mean (log mg/l) | 19 | 5 1 95 | 1 95 | 1 95 | 1 95 | 1 95 | 13 | 2 43 | 2 15 | 24 | 3 24 | 3 1 3 | 2 2 4 | 3 2 15 | 2 43 | 2.43 | 13 | 2 4 | 2 15 | 24 | 3 2 43 | 1 95 | 1 95 | 1 95 | 1 95 | 1 95 |
| Stormflow Total Suspended Solids Standard Deviation (log mg/L) | 0.3 | 2 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 2 03 | 2 03 | 2 033 | 2.1 | 2 0 32 | 0.32 | 0.32 | 0 32 | 0.3 | 2.13 | 0.3 | 2 0 32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 |
| Stormflow Total Suspended Solids Estimation Method | Stochasti | ir Stochastic | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | r Stochasti | r Stochasti | r Stochasti | Stochasti | c Stochastic 9 | Stochastic | Stochasti | Stochastic | Storhasti | Stochastic | Storhasti | r Stochastic | Stochastic S | torhastic | Stochastic | Stochastic | Stochastic |
| Stormflow Total Suspended Solids Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | 0 | 0 | C | 0 | Geochasti | 0 0 | Stotnusti | 0 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Phosphorus Mean (log mg/l) | -0.6 | 6 -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.89 | -0.3 | -0.6 | -03 | -03 | -0.80 | -03 | 3 -0.6 | -03 | -03 | -0.89 | -0 3 | -06 | -0 3 | 2 -03 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 |
| Stormflow Total Phosphorus Standard Deviation (log mg/L) | 0.2 | 5 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.5 | 0.25 | 0.2 | 5 0.25 | 5 0.05 | 0.2 | 5 0.25 | 0.5 | 0.25 | 0.05 | 0.25 | 0.0 | 0.2 | 5 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Stormflow Total Phosphorus Estimation Method | Stochasti | ir Stochastir | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | r Stochasti | r Stochasti | r Stochasti | Storhasti | c Stochastic 9 | Stochastic | Stochasti | Stochastic | Storhasti | Stochastic | Storhasti | r Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic |
| Stormflow Total Phosphorus Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (|) (|) (|) (|) 0 | 0 | C | 0 | Geochasti | 0 0 | (| 0 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Nitrogen Mean (log mg/l) | 0 | 3 03 | 03 | 03 | 03 | 03 | 03 | 0 34 | 03 | 1 034 | 1 034 | 1 03 | 0.34 | 1 03 | 0 34 | 0.34 | 03 | 0.34 | 1 03 | 0.34 | 1 034 | 03 | 03 | 03 | 03 | 03 |
| Stormflow Total Nitrogen Standard Deviation (log mg/l) | 0.1 | 9 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Stormflow Total Nitrogen Estimation Method | Stochasti | ir Stochastir | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | r Stochasti | r Stochasti | r Stochasti | Storhasti | r Stochastic | Storhastir | Stochasti | Stochastic | Storhasti | Stochastic | Storhasti | r Stochastic | Stochastic S | torhastir | Stochastic | Stochastic | Stochastic |
| Stormflow Total Nitrogen Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | | | 0 | 0 | C | 0 | Geochasti | 0 0 | Stotnusti | 0 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Suspended Solids Mean (log mg/L) | 1.1 | 5 115 | 1 15 | 1 15 | 1 15 | 1 15 | 12 | 12 | 12 | 1 | 11 | 2 12 | 12 | 2 12 | 12 | 12 | 12 | 12 | 12 | 13 | 2 12 | 1 15 | 1 15 | 1 15 | 1 15 | 1 15 |
| Baseflow Total Suspended Solids Standard Deviation (log mg/L) | 0.1 | 7 0 17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 7 0.1 | 7 0.17 | 7 0.17 | 0.17 | 7 0 17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.1 | 7 0 17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Baseflow Total Suspended Solids Estimation Method | Stochasti | r Stochastic | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | r Stochasti | r Stochasti | r Stochasti | Storhasti | r Stochastic | Storhastir | Stochasti | Stochastic | Storhasti | Stochastic | Storhasti | r Stochastic | Stochastic S | torhastir | Stochastic | Stochastic | Stochastic |
| Baseflow Total Suspended Solids Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | 0 | 0 | C | 0 | Geochasti | 0 0 | Stochasti | 0 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Phosphorus Mean (log mg/l) | -1.2 | 2 -1 22 | -1 22 | -1 22 | -1 22 | -1 22 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -1 22 | -1 22 | -1 22 | -1 22 | -1 22 |
| Baseflow Total Phosphorus Standard Deviation (log mg/L) | 0.1 | 0 0 10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.05 | 0.05 | 0.03 | 0.0 | 0.02 | 0.02 | 0.02 | 0.05 | 0.05 | 0.03 | 0.05 | 0.02 | 0.05 | 0.0 | 0.05 | 0.10 | 0.19 | 0.10 | 0.10 | 0.10 |
| Baseflow Total Phoenborus Estimation Method | Stochasti | ir Stochastir | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | c Stochasti | c Stochasti | c Stochasti | Stochasti | c Stochastic St | tochastic | Stochasti | Stochastic | Stochasti | Stochastic | Stochasti | c Stochastic | Stochastic | tochastic | Stochastic | Stochastic | Stochastic |
| Baseflow Total Phosphorus Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 00000000 | 0 | | | | | | nocinastic 0 | C | | Stochasti | | Stochasti | | 0 | n | 0 | 0 | 0 |
| Baseflow Total Nitrogen Mean (log mg/l) | -0.0 | 5 -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | 0.11 | 0 11 | 0.11 | 0.11 | 0 11 | 0 11 | 0.11 | 0 11 | 0.11 | 0.11 | 0 11 | 0.11 | 0 11 | 0.11 | 0 11 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 |
| Baseflow Total Nitrogen Standard Deviation (log mg/l) | 0.0 | 2 0.12 | 0.03 | 0.03 | 0.03 | 0.03 | 0.12 | 0.12 | 0.12 | 0.1 | 0.12 | 2 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| Baseflow Total Nitrogen Standard Deviation (log mg/c) | Stochasti | ir Stochastir | Stochastic | Stochastic | Stochastic | Stochastic | Stochastic St | ochastic | Stochasti | stochasti | c Stochasti | c Stochasti | Stochasti | c Stochastic 9 | torbastir | Stochasti | Stochastic | Stochasti | Stochastic | Stochasti | c Stochastic | Stochastic | tochastic | Stochastic | Stochastic | Stochastic |
| Baseflow Total Nitrogen Serial Correlation | Stochast | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | 0 | C | 0 | Scoenaser (| 0 | Stotnusti | | 0 | 0 | 0 | 0 | 0 |
| Elow based constituent generation - enabled | Off | Off | Off | Off | Off | Off | Off O | ff (| Off | Off | , Cff | , C | Off | , Off (| off U | Off | Off | Off | Off | Off | , Off | Off | off | Off | Off | Off |
| Flow based constituent generation - enabled | UII | UII | UII | 011 | UII | UII | 011 0 | | on | UII | UII | UII | UII | UII (| 511 | 011 | UII | 011 | UII | UII | UII | 011 0 | /11 | 011 | on | UII |
| Flow based constituent generation - how me | - | | | | | | | | | | | | - | | | | | | | | | | | | | |
| Flow based constituent generation - base flow column | - | | | | | | | | | | | | - | | | | | | - | | | | | | | |
| Flow based constituent generation - pervicus now column | - | | | | | | | | | | | | - | | | | | | - | | | | | | | |
| Flow based constituent generation - impervious flow column | | | | | | | | | | | | | | | | | | | | | | | | | | |
| riow based constituent generation - unit | | _ | | | | | | | | | | | | | | | | ļ | | | | | | | | |



Table B-10: UTSM treatment nodes – Sydney Water - East cluster

| | Wetland | Wetland | Wetland | Pond 25 + | | Pond | H02a_Op | E01_Op4 | E02_Op4 | E02_Bior | E01_Bior | E03_Bior | Wetland | Copy of Wetland | Copy of Wetland |
|--|----------------|---------------|----------|-------------------|------------------|------------------|-----------|----------------|----------------|----------------|-----------------|----------------|------------|--------------------|--------------------|
| Location | 25 + 26 | 28 | 29+30+31 | 26 | Pond 28 | 29+30+31 | 4_StTr | _StTr | _StTr | etention | etention | etention | 28 | 25 + 26 | 28 |
| ID Nodo Turo | 24 Wotlands | 25 | 26 | 27 RondNod | 28 RondNod | BondNod | 9 30 | 31 BioRoton | 32 BioRoton | 45 BioRotop | 46 BioRotopt | 47 RicPoton | 54 Wotland | 55 Wotland | 56 56 |
| lo-flow bypass rate (cum/sec) | 0 | overanuk 0 | 0 O | 0 | C | | | O | O | O | 0 | BIORELEII | | wettanur | |
| Hi-flow bypass rate (cum/sec) | 4 | 5 | 5 | 100 | 100 | 0 100 | 0.271 | 0.075 | 0.037 | 100 | 100 | 100 | 66 | 4 | 1 5 |
| Inlet pond volume | 2751.8 | 1542.2 | 5727 | 0 | C 5440 7 | 0 (|) 1707.50 | 407.52 | 240.22 | 2244 | 0250.2 | 21120 | 1226 | 6005 7 | 0 0 |
| Initial Volume (m^3) | 785 | 461 | 6480 | 27148 | 6808 | 4998: 3 78454 | 1/97.59 | 497.53 | 248.32 | 3344 | 9359.3 | 31138 | 739 | 785 | 3357.5 461 |
| Extended detention depth (m) | 0.02 | 0.01 | 0.05 | 0.05 | 0.05 | 5 O.1 | L 0.02 | 0.02 | 0.02 | 0.3 | 0.3 | 0.3 | 0.01 | 0.3 | 8 0.3 |
| Number of Rainwater tanks | 205 | | <i></i> | | | | | | | | | | | 205 | |
| Permanent Pool Volume (cubic metres) Proportion vegetated | 785 | 461 | 6480 | 27148 | 6808 | 3 78454 | 1 | | | | | | 739 | 785 | 5 461 5 0.5 |
| Equivalent Pipe Diameter (mm) | 46 | 29 | 112 | 199 | 120 |) 434 | 1 | | | | | | 25 | 90 | 0.5 |
| Overflow weir width (m) | 10 | 10 | 80 | 10 | 10 |) 20 |) 2 | 2 | 2 | 8 | 8 | 20 | 10 | 10 | 0 10 |
| Notional Detention Time (hrs) | 47.9 | 47.6 | 48.8 | 10 | 10.1 | 10 | 2 | | | | | | 47 | 48.4 | 47.4 |
| Weir Coefficient | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 7 1.7 | 7 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 7 1.7 |
| Number of CSTR Cells | 2 | 2 | 2 | 2 | 2 | 2 2 | 2 3 | 3 | 3 | 3 | 3 | 3 | 8 2 | 2 | 2 2 |
| Total Suspended Solids - k (m/yr) | 1500 | 1500 | 1500 | 400 | 400 | 0 400 | 8000 | 8000 | 8000 | 8000 | 8000 | 8000 | 1500 | 1500 | 1500 |
| Total Suspended Solids - C* (mg/L) | 6 | 6 | 6 | 12 | 12 | 2 1. | 2 20 | 20 | 20 | 20 | 20 | 20 | 6 | e e | 5 6 |
| Total Phosphorus - k (m/yr) | 1000 | 1000 | 1000 | 300 | 300 | 300 | 6000 | 6000 | 6000 | 6000 | 6000 | 6000 | 1000 | 1000 | 1000 |
| Total Phosphorus - C* (mg/L) | 0.06 | 0.06 | 0.06 | 0.09 | 0.09 | 0.09 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.06 | 0.06 | 5 0.06 |
| Total Phosphorus - C** (mg/L) | 0.06 | 0.06 | 0.06 | 0.09 | 0.09 | 9 0.09 | 9 500 | 500 | 500 | 500 | 500 | 500 | 0.06 | 0.06 | 5 0.06 1 150 |
| Total Nitrogen - C* (mg/L) | 130 | . 130 | 130 | | . 1 | 1 : | 1 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 130 | . 150 | L 1 |
| Total Nitrogen - C** (mg/L) | 1 | . 1 | . 1 | 1 | . 1 | 1 : | 1 | | | | | | 1 | . 1 | ι 1 |
| Threshold Hydraulic Loading for C** (m/yr) | 3500 | 3500 | 3500 | 3500 | 3500 | 3500 |) | 2 | 2 | 2 | - | | 3500 | 3500 | 3500 |
| Reuse Enabled | Off | Off | Off | On | On | On | Off | 3 Off | 3 Off | Off 3 | 3 Off | Off | Off | Off | Off |
| Max drawdown height (m) | | | | 1.820619 | 1.25131 | 1.569614 | 1 | | | | | | | | |
| Annual Demand Enabled | Off | Off | Off | On | On | On | Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Annual Demand Value (ML/year) | | | | 19.223 Monthly | 8.753 Monthly | Monthly | <u>'</u> | | | | | | | | |
| Annual Demand Monthly Distribution: Jan | | | | 13 | 13 | 3 13 | 3 | | | | | | | | |
| Annual Demand Monthly Distribution: Feb | | | | 6 | ε | 5 6 | 5 | | | | | | | | |
| Annual Demand Monthly Distribution: Mar | | | | 6 | e | 5 6 | 5 | | | | | | | | |
| Annual Demand Monthly Distribution: Apr | | | | 2 | 2 | 2 2 | 2 | | | | | | | | |
| Annual Demand Monthly Distribution: Jun | | | | 0 | 0 |) (|) | | | | | | | | |
| Annual Demand Monthly Distribution: Jul | | | | 4 | 4 | 1 4 | 1 | | | | | | | | |
| Annual Demand Monthly Distribution: Aug | | | | 12 | 12 | 2 12 | , > | | | | | | | | |
| Annual Demand Monthly Distribution: Oct | | | | 14 | - 14 | 1 14 | 1 | | | | | | | | |
| Annual Demand Monthly Distribution: Nov | | | | 13 | 13 | 3 13 | 3 | | | | | | | | |
| Annual Demand Monthly Distribution: Dec | Off | Off | Off | 19 | 0n 19 | 9 19 |) Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Daily Demand Value (ML/day) | UII | UII | UII | 0.121 | 0.06 | 5 0.433 | 7 | UII | UII | UII | UII | UII | on | on | on |
| Custom Demand Enabled | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Custom Demand Time Series File | | | | | | | | | | | | | | | |
| Filter area (sgm) | | | | | | | 1797.59 | 497.53 | 248.32 | 880 | 2463 | 8176 | 5 | | |
| Filter perimeter (m) | | | | | | | 0.01 | 0.01 | 0.01 | . 14 | 14 | 14 | l . | | |
| Filter depth (m) | | | | | | | 0.52 | 0.52 | 0.52 | 0.5 | 0.5 | 0.5 | | | |
| Filter Median Particle Diameter (mm) Saturated Hydraulic Conductivity (mm/hr) | | | | | | | 25 | 25 | 25 | 100 | 100 | 100 |) | | |
| Infiltration Media Porosity | | | | | | | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | | | |
| Length (m) | | | | | | | | | | | | | | | |
| Bed Slope Base Width (m) | | | | | | | | | | | | | | | |
| Top width (m) | | | | | | | | | | | | | | | |
| Vegetation height (m) | | | | | | | | | | | | | | | |
| Vegetation Type | | | | | | | Vegetate | Vegetate | Vegetate | Vegetate | Vegetated | Vegetate | ¢ | | |
| Orthophosphate Content in Filter (mg/kg) | | | | | | | 400 | 400 | 400 | 400 | 400 | 900 |) | | |
| Is Base Lined? | | | | | | | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| Is Underdrain Present? | | | | | | | Yes | Yes | Yes | Yes | Yes | Yes | | | |
| Is Submerged Zone Present? | | | | | | | NO | NO | NO | NO | NO | NO | | | |
| B for Media Soil Texture | -9999 | -9999 | -9999 | -9999 | -9999 | -9999 | 9 13 | 13 | 13 | 13 | 13 | 13 | -9999 | -9999 | -9999 |
| Proportion of upstream impervious area treate | | | | | | | | | | | | | | | |
| Exfiltration Rate (mm/hr) | 0 | 0 | 125 | 100 | 100 |) (| 0 0 | 100 | 100 | 100 | 0 | 100 | 125 | 0 | 0 0 |
| Depth in metres below the drain pipe | 30 | | 125 | 100 | 100 | , 100 | , 100 | 100 | 100 | 100 | 100 | 100 | . 125 | 50 | |
| TSS A Coefficient | | | | | | | | | | | | | | | |
| TSS B Coefficient | | | | | | | | | | | | | | | |
| TP B Coefficient | | | | | | | | | | | | | | | |
| TN A Coefficient | | | | | | | | | | | | | | | |
| TN B Coefficient | | | | | | | | | | | | | | | |
| STC S* | | | | | | | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | , | | |
| Św | | | | | | | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | L | | |
| Sh | | | | | | | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 5 | | |
| Emax (m/day) | | | | | | | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 8 | | |
| cw (III/day) | | | | | | | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | - | | |



| | H02a_Lot | E01_Lot_ | H02c_Lot |
|--|----------|----------|----------|
| Location | _GPT | GPT | _GPT |
| ID | 42 | 43 | 44 |
| Node Type | GPTNode | GPTNode | GPTNode |
| Lo-flow bypass rate (cum/sec) | 0 | 0 | 0 |
| Hi-flow bypass rate (cum/sec) | 1.84 | 0.46 | 0.25 |
| Flow Transfer Function | | | |
| Input (cum/sec) | 0 | 0 | 0 |
| Output (cum/sec) | 0 | 0 | 0 |
| Input (cum/sec) | 10 | 10 | 10 |
| Output (cum/sec) | 10 | 10 | 10 |
| Gross Pollutant Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (kg/ML) | 0 | 0 | 0 |
| Output (kg/ML) | 0 | 0 | 0 |
| Input (kg/ML) | 100 | 100 | 100 |
| Output (kg/ML) | 2 | 2 | 2 |
| Total Nitrogen Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 50 | 50 | 50 |
| Output (mg/L) | 50 | 50 | 50 |
| Total Phosphorus Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 0.5 | 0.5 | 0.5 |
| Output (mg/L) | 0.5 | 0.5 | 0.5 |
| Input (mg/L) | 10 | 10 | 10 |
| Output (mg/L) | 7 | 7 | 7 |
| Total Suspended Solids Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 75 | 75 | 75 |
| Output (mg/L) | 75 | 75 | 75 |
| Input (mg/L) | 1000 | 1000 | 1000 |
| Output (mg/l) | 300 | 300 | 300 |
| TSS Flow based Efficiency Enabled | Off | Off | Off |
| TSS Flow based Efficiency | | | • |
| TP Flow based Efficiency Enabled | Off | Off | Off |
| TP Flow based Efficiency | | | |
| TN Flow based Efficiency Enabled | Off | Off | Off |
| TN Flow based Efficiency | | | |
| GP Flow based Efficiency Enabled | Off | Off | Off |
| GP Flow based Efficiency | | | |
| | | | |

Table B-11: Generic treatment nodes - Sydney Water - East cluster



Table B-12: Other nodes - Sydney Water - East cluster

| | Wetland | | | Pond | | | | | | | | | Note on |
|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|
| | 1 - | H02a_LO | E01_LOT_ | 29+30+31 | E02_LOT_ | Pond 28 | | Ropes | | E01 Trunk | E02 Trunk | E03 Trunk | sed |
| Location | Median | T_Jnc | Jnc | Report | Jnc | Report | Junction | Creek | Junction | Drainage | Drainage | Drainage | basins |
| ID | 33 | 34 | 35 | 36 | 5 37 | 38 | 39 | 40 | 41 | 48 | 50 | 52 | 57 |
| Node Type | JunctionN | JunctionN | JunctionN | Junction | JunctionN | Junction | JunctionN | Junction | JunctionN | JunctionN | JunctionN | JunctionN | JunctionN |



B.2.4 TWG stormwater consultant East Cluster Alternative 3

Table B-13: Source node information – TWG stormwater consultant - East cluster

| | | | | | | Wetland | | | | | | | | | | | | | | | | | Pond | | | Bio | | | | |
|--|------------|-----------|------------|--------------|-----------|------------|--------------|------------|------------|------------|----------|------------|-----------|--------------|-------------|------------|--------------|-------------|--------------|---------------|--------------|------------|------------|------------|------------|------------|------------|--------------|------------|------------|
| | | Wetland | Pond 25 | Wetland P | ond 28 | 29+30+31 | E03_100 | | E03_Lot_ | | | E01_100 | | E01_Lot_ | | | E02_100 | | E02_Lot_ | | | | 29+30+31 | Bio 25 | Bio 28 | 29+30+31 | GAINED | | | |
| | E01_int_ | 25 direct | direct | 28 direct | irect | direct | %_Lot_R E | E03_Lot_ | Landscap | E03_St_P | 03_St_P | %_Lot_R | E01_Lot | Landscap | E01_St_F | E01_St_ | P %_Lot_R | E02_Lot | Landscap | E02_St_P | 5.180_St_ | E_ext_PO | direct | direct | direct | direct | AREA | EASEMEN / | EASEMEN | EASEMEN |
| Location | POS | rainfall | rainfall | rainfall r | ainfall | rainfall | oof F | Pave | e | ave e | rv | oof | Pave | e | ave | erv | oof | Pave | e | ave | Perv | s | rainfall | rainfall | rainfall | rainfall | ALT3 | T ' | r ' | т |
| ID | 1 | . 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 1 | 3 1 | 4 1 | 5 1 | L6 1 | 7 1 | 8 19 | 20 | 0 21 | 22 | 23 | 47 | 49 | 51 | 54 | 57 | 58 | 59 |
| Node Type | UrbanSou | UrbanSou | urbanSou | UrbanSou L | IrbanSou | UrbanSou | UrbanSou l | JrbanSou | UrbanSou | UrbanSou I | IrbanSou | UrbanSou | UrbanSo | u UrbanSo | u UrbanSo | u UrbanSc | u UrbanSo | u UrbanSo | u UrbanSou | u UrbanSou | u UrbanSou | UrbanSou ! | UrbanSou | UrbanSou |
| Zoning Surface Type | Revegeta | Revegeta | Revegeta | Revegetal P | evegetat | Revegetat | Roof I | ndustrial | Industrial | Sealedroa | ealedro | Roof | Industria | al Industria | I Sealedro | oa Sealedr | oa Roof | Industria | al Industria | Sealedro | a Sealedroa | Revegetat | Revegetat | Revegetat | Revegetat | Revegetat | Revegetat | Revegetat / | Revegetat | Revegetat |
| Total Area (ha) | 10.23 | 0.577 | 1.606 | 0.274 | 0.542 | 2.236 | 57.651 | 31.446 | 15.723 | 5.33 | 1.64 | 13.101 | 7.14 | 6 3.57 | 3 3.8 | 5 1.1 | 18 6.95 | 2 3.79 | 2 1.896 | 5 0.81 | 1 0.25 | 51.62 | 4.997 | 0.173 | 0.082 | 0.575 | 3.55 | 3 | 2.2 | 3.3 |
| Area Impervious (ha) | 0 | 0.23009 | 1.4454 | 0.109263 | 0.4878 | 0.900073 | 57.651 | 31.446 | 0 | 5.33 | C | 13.101 | 7.14 | 6 | 0 3.8 | 15 | 0 6.95 | 2 3.79 | 2 (| 0.81 | 1 0 | 0 | 4.507369 | 0 | 0 | 0 | 0.695694 | 0.58791 | 0.431134 | 0.646701 |
| Area Pervious (ha) | 10.23 | 0.34691 | 0.1606 | 0.164737 | 0.0542 | 1.335927 | 0 | 0 | 15.723 | 0 | 1.64 | 0 | | 0 3.57 | 3 | 0 1.1 | 18 | 0 | 0 1.896 | 5 (| 0.25 | 51.62 | 0.489631 | 0.173 | 0.082 | 0.575 | 2.854306 | 2.41209 | 1.768866 | 2.653299 |
| Field Capacity (mm) | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 13 | 0 13 | 0 13 | 0 13 | 30 13 | 0 13 | 0 130 | 130 | 0 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 |
| Pervious Area Infiltration Capacity coefficient - a | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 17 | 5 17 | 5 17 | 5 17 | 75 17 | 5 17 | 5 175 | 5 175 | 5 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 | 175 |
| Pervious Area Infiltration Capacity exponent - b | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2. | 5 2. | 5 2. | .5 2 | .5 2. | 5 2. | 5 2.5 | 5 2.5 | 5 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| Impervious Area Rainfall Threshold (mm/day) | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | 1 | 1 | 1 | 1 | 1 | 1 : | 1 : | 1 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Pervious Area Soil Storage Capacity (mm) | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 15 | 0 15 | 0 15 | 0 1 | 50 15 | 0 15 | 0 150 |) 150 | 0 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 |
| Pervious Area Soil Initial Storage (% of Capacity) | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 1 3 | ю з | 0 3 | 0 3 | 30 3 | 0 3 | 0 30 | 30 | 0 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| Groundwater Initial Depth (mm) | 10 | 10 | 0 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |) 1 | 0 1 | 0 1 | 0 | 10 1 | 0 1 | .0 10 | 0 10 | 0 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| Groundwater Daily Recharge Rate (%) | 25 | 5 25 | 5 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 1 2 | 25 2 | 5 2 | 25 | 25 2 | 5 2 | 5 2 | 5 2 | 5 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| Groundwater Daily Baseflow Rate (%) | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1 | 4 1. | 4 1 | 4 1 | .4 1 | 4 1 | 4 1.4 | 4 1.4 | 4 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Groundwater Daily Deep Seepage Rate (%) | C |) (|) (| 0 | 0 | 0 | 0 | 0 | C | 0 0 | (| 0 0 |) | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Suspended Solids Mean (log mg/L) | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.3 | 2.43 | 2.15 | 2.43 | 2.43 | 1.3 | 2.4 | 3 2.1 | 5 2.4 | 3 2.4 | 13 1. | 3 2.4 | 3 2.15 | 2.43 | 3 2.43 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| Stormflow Total Suspended Solids Standard Deviation (log mg/L) | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.3 | 2 0.3 | 2 0.3 | 2 0.3 | 32 0.3 | 2 0.3 | 2 0.32 | 2 0.32 | 2 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 |
| Stormflow Total Suspended Solids Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic ' | Stochastic | Stochastic |
| Stormflow Total Suspended Solids Serial Correlation | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Phosphorus Mean (log mg/L) | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.89 | -0.3 | -0.6 | -0.3 | -0.3 | -0.89 | -0. | 3 -0. | 6 -0. | .3 -0 | .3 -0.8 | 9 -0. | 3 -0.6 | -0.3 | 3 -0.3 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 | -0.66 |
| Stormflow Total Phosphorus Standard Deviation (log mg/L) | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.2 | 5 0.2 | 5 0.2 | 5 0.2 | 25 0.2 | 5 0.2 | 5 0.25 | 5 0.25 | 5 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| Stormflow Total Phosphorus Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic S | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic ' | Stochastic | Stochastic |
| Stormflow Total Phosphorus Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stormflow Total Nitrogen Mean (log mg/L) | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.34 | 0.3 | 0.34 | 0.34 | 0.3 | 0.3 | 4 0. | 3 0.3 | 4 0.3 | 34 0. | 3 0.3 | 4 0.3 | 3 0.34 | 4 0.34 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| Stormflow Total Nitrogen Standard Deviation (log mg/L) | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.1 | 9 0.1 | 9 0.1 | .9 0.1 | 19 0.1 | 9 0.1 | 9 0.19 | 0.19 | 9 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Stormflow Total Nitrogen Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic' | Stochastic | Stochastic |
| Stormflow Total Nitrogen Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Suspended Solids Mean (log mg/L) | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1. | 2 1. | 2 1. | 2 1 | .2 1. | 2 1. | 2 1.2 | 2 1.2 | 2 1.2 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 | 1.15 |
| Baseflow Total Suspended Solids Standard Deviation (log mg/L) | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.1 | 7 0.1 | 7 0.1 | 7 0.1 | 17 0.1 | 7 0.1 | 7 0.17 | 0.17 | 7 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Baseflow Total Suspended Solids Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic' | Stochastic | Stochastic |
| Baseflow Total Suspended Solids Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Phosphorus Mean (log mg/L) | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.85 | -0.8 | 5 -0.8 | 5 -0.8 | -0.8 | -0.8 | 5 -0.8 | 5 -0.85 | -0.85 | 5 -0.85 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 | -1.22 |
| Baseflow Total Phosphorus Standard Deviation (log mg/L) | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.1 | 9 0.1 | 9 0.1 | .9 0.1 | 19 0.1 | 9 0.1 | 9 0.19 | 0.19 | 9 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Baseflow Total Phosphorus Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic' | Stochastic | Stochastic |
| Baseflow Total Phosphorus Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baseflow Total Nitrogen Mean (log mg/L) | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | 0.1 | 1 0.1 | 1 0.1 | 1 0.1 | 1 0.1 | 1 0.1 | 1 0.11 | 0.11 | 1 0.11 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 |
| Baseflow Total Nitrogen Standard Deviation (log mg/L) | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.1 | 2 0.1 | 2 0.1 | 2 0.1 | 12 0.1 | 2 0.1 | 2 0.12 | 0.12 | 2 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| Baseflow Total Nitrogen Estimation Method | Stochastie | Stochasti | Stochastic | Stochastic S | tochastic | Stochastic | Stochastic | Stochastic | Stochasti | Stochastic | tochasti | Stochastic | Stochast | ic Stochast | ic Stochast | ic Stochas | tic Stochast | ic Stochast | ic Stochasti | c Stochasti | c Stochastic | Stochastic' | Stochastic | Stochastic |
| Baseflow Total Nitrogen Serial Correlation | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 |) (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Flow based constituent generation - enabled | Off | Off | Off | Off (| Off | Off | Off (| Off | Off | Off (| off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off (| Off | Off |
| Flow based constituent generation - flow file | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - base flow column | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - pervious flow column | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - impervious flow column | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow based constituent generation - unit | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| · · · · · · · · · · · · · · · · · · · | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |



Table B-14: UTSM treatment nodes – TWG stormwater consultant - East cluster

| | Wetland | Wetland | Pond 25+ | | Pond | H02a_Op | E01_Op4 | E02_Op4 | | E03_Bior | Wetland | |
|--|---------|----------|-----------|----------|-----------|-----------|----------|----------|-----------|------------|---------|----------|
| Location | 28 | 29+30+31 | 26 | Pond 28 | 29+30+31 | 4_StTr | _StTr | _StTr | 25-26 Bio | etention | 25 + 26 | 28 Bio |
| ID | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 44 | 45 | 53 | 55 |
| Node Type | Wetland | WetlandN | PondNod | PondNod | PondNod | BioRetent | BioReten | BioReten | BioReten | t BioReten | Wetland | BioReten |
| Lo-flow bypass rate (cum/sec) | 0 | 0 | 0 | 100 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HI-flow bypass rate (cum/sec) | 5 | 4472 | 100 | 100 | 100 | 0.2/1 | 0.075 | 0.037 | 100 | 100 | 4 | 100 |
| | 246 | 20122 | 12216 | 2061 | 25000 | 1707 50 | 407 52 | 249.22 | 7501 | 20065 | 5102 | 2562 |
| Initial Volume (mA2) | 2400 | 6707 | 24422 | 5022 | 70000 | 1/97.59 | 497.55 | 240.32 | 7501 | 29005 | 1721 | 5502 |
| Extended detention denth (m) | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.02 | 0.02 | 0.02 | 03 | 03 | 0.05 | 03 |
| Number of Bainwater tanks | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.02 | 0.02 | 0.02 | 0.5 | 0.5 | 0.05 | 0.5 |
| Permanent Pool Volume (cubic metres) | 822 | 6707 | 24433 | 5923 | 70000 |) | | | | | 1731 | |
| Proportion vegetated | 0.5 | 0.5 | 0.1 | 0.1 | 0.1 | | | | | | 0.5 | |
| Equivalent Pipe Diameter (mm) | 37 | 106 | 199 | 120 | 434 | Ļ | | | | | 54 | |
| Overflow weir width (m) | 10 | 80 | 10 | 10 | 20 | 2 | 2 | 2 | 25 | 20 | 10 | 25 |
| Notional Detention Time (hrs) | 48 | 47.7 | 8.22 | 5.48 | 4.95 | ; | | | | | 47.5 | |
| Orifice Discharge Coefficient | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | i | | | | | 0.6 | |
| Weir Coefficient | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 |
| Number of CSTR Cells | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 2 | 3 |
| Total Suspended Solids - k (m/yr) | 1500 | 1500 | 400 | 400 | 400 | 8000 | 8000 | 8000 | 8000 | 8000 | 1500 | 8000 |
| Total Suspended Solids - C* (mg/L) | 6 | 6 | 12 | 12 | 12 | 20 | 20 | 20 | 20 | 20 | 6 | 20 |
| Total Suspended Solids - C** (mg/L) | 6 | 6 | 12 | 12 | 12 | 2 | | | | | 6 | |
| Total Phosphorus - k (m/yr) | 1000 | 1000 | 300 | 300 | 300 | 6000 | 6000 | 6000 | 6000 | 6000 | 1000 | 6000 |
| Total Phosphorus - C* (mg/L) | 0.06 | 0.06 | 0.09 | 0.09 | 0.09 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.06 | 0.13 |
| Total Phosphorus - C** (mg/L) | 0.06 | 0.06 | 0.09 | 0.09 | 0.09 |) | | | | | 0.06 | |
| Total Nitrogen - k (m/yr) | 150 | 150 | 40 | 40 | 40 | 500 | 500 | 500 | 500 | 500 | 150 | 500 |
| Total Nitrogen - C* (mg/L) | 1 | 1 | 1 | . 1 | . 1 | . 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1 | 1.4 |
| I otal Nitrogen - C** (mg/L) | 1 | 1 | 1 | 1 | . 1 | | | | | | 1 | |
| Inreshold Hydraulic Loading for C** (m/yr) | 3500 | 3500 | 3500 | 3500 | 3500 |) | | | | | 3500 | |
| Horizontal Flow Coefficient | 04 | 04 | 0 | 0- | 0- | 3 | 3 | 3 | 3 | 3 | 04 | 3 |
| Keuse Enabled | UT | UTT | Un 1.000 | Un - | Un - | UTT | UTT | UTT | UTT | UTT | UTT | UTT |
| Max drawdown height (m) | | | 1.999 | 2 | 2 | | | | | | | |
| Annual Demand Enabled | Off | Off | On 10 222 | On 0.752 | On cc oor | Off | Off | Off | Off | Off | Off | Off |
| Annual Demand Value (ML/year) | | | 19.223 | 8./53 | 5 66.002 | | | | | | | |
| Annual Demand Monthly Distribution | | | 12 | wonthiy | 12 | | | | | | | |
| Annual Demand Monthly Distribution: Jan | | | 13 | 13 | 13 | | | | | | | |
| Annual Demand Monthly Distribution: Nar | | | 6 | 6 | 6 | | | | | | | |
| Annual Demand Monthly Distribution: Ann | | | 0 | | 1 | 1 | | | | | | |
| Annual Demand Monthly Distribution: May | | | - 4 | 2 | 2 | • | | | | | | |
| Annual Demand Monthly Distribution: Jun | | | 0 | 2 | 1 0 | • | | | | | | |
| Annual Demand Monthly Distribution: Jul | | | 4 | | | • | | | | | | |
| Annual Demand Monthly Distribution: Aug | | | 7 | 7 | · | ; ; | | | | | | |
| Annual Demand Monthly Distribution: Sep | | | . 12 | 12 | 12 | , | | | | | | |
| Annual Demand Monthly Distribution: Oct | | | 14 | 14 | 14 | | | | | | | |
| Annual Demand Monthly Distribution: Nov | | | 13 | 13 | 13 | | | | | | | |
| Annual Demand Monthly Distribution: Dec | | | 19 | 19 | 19 |) | | | | | | |
| Daily Demand Enabled | Off | Off | On | On | On | Off | Off | Off | Off | Off | Off | Off |
| Daily Demand Value (ML/day) | | | 0.1089 | 0.0522 | 0.424 | L | | | | | | |
| Custom Demand Enabled | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off | Off |
| Custom Demand Time Series File | | | | | | | | | | | | |
| Custom Demand Time Series Units | | | | | | | | | | | | |
| Filter area (sqm) | | | | | | 1797.59 | 497.53 | 248.32 | 1731 | . 6707 | | 822 |
| Filter perimeter (m) | | | | | | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | | 0.01 |
| Filter depth (m) | | | | | | 0.52 | 0.52 | 0.52 | 0.5 | 0.5 | | 0.5 |
| Filter Median Particle Diameter (mm) | | | | | | | | | | | | |
| Saturated Hydraulic Conductivity (mm/hr) | | | | | | 25 | 25 | 25 | 100 | 100 | | 100 |
| Infiltration Media Porosity | | | | | | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | | 0.35 |
| Length (m) | | | | | | | | | | | | |
| Bed slope | | | | | | | | | | | | |
| Base Width (m) | | | | | | | | | | | | |
| lop width (m) | | | | | | | | | | | | |
| Vegetation height (m) | | | | | | N | | | | | | |
| Vegetation Type | | | | | | Vegetated | Vegetate | Vegetate | Vegetate | Vegetate | 1 | Vegetate |
| Orthon house to content in Filter (mg/kg) | - | | | | | 400 | 400 | 400 | 400 | 900 | | 400 |
| Untriophosphate Content in Filter (mg/kg) | - | | | | | 40 | 40 | 40 | 40 | 40 | | 40 |
| Is base Lined? | | | | | | res | TES | res | res | res | | res |
| Is onderuran riesent? | | | | | | No | No | No | Voc | Voc | | Voc |
| Submerged Zone Depth (m) | | | | | | NU | NU | NU | 105 | 105 | | 105 |
| Submerged Zone Depth (m) | - 0000 | -0000 | -0000 | -0000 | -0000 | 12 | 12 | 12 | 0.3 | 0.3 | -0000 | 0.3 |
| Broportion of unstream impensious area treated | - 55555 | -3555 | -5555 | -5555 | | , 13 | 15 | 13 | 13 | 1.5 | - 3555 | 13 |
| Excitization Pate (mm/br) | 0.01 | 0.01 | 0 | | | 0 | 0 | 0 | 0 | 0 | 0.01 | 0 |
| Evanorative Loss as % of PET | 125 | 125 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 125 | 100 |
| Depth in metres below the drain nine | 125 | 125 | 100 | 100 | , 100 | 100 | 100 | 100 | 100 | 100 | 125 | 100 |
| TSS A Coefficient | | | | | | | | | | | | |
| TSS B Coefficient | | | | | | | | | | | | |
| TP A Coefficient | | | | | | | | | | | | |
| TP B Coefficient | | | | | | | | | | | | |
| TN A Coefficient | | | | | | | | | | | | |
| TN B Coefficient | | | | | | | | | | | | |
| Sfc | | | | | | 0.61 | 0.61 | 0.61 | 0.61 | 0.61 | | 0.61 |
| S* | | | | | | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | | 0.37 |
| Sw | | | | | | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 | | 0.11 |
| Sh | | | | | | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | | 0.05 |
| Emax (m/day) | | | | | | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | | 0.008 |
| Ew (m/day) | | | | | | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | | 0.001 |
| | | | | | | | | | | | | |



Table B-15: Generic treatment nodes – TWG stormwater consultant - East cluster H02a_Lot E01_Lot_ H02c_Lot GDT CDT CDT

| Location | _GPT | GPT | _GPT |
|--|---------|---------|---------|
| ID | 41 | 42 | 43 |
| Node Type | GPTNode | GPTNode | GPTNode |
| Lo-flow bypass rate (cum/sec) | 0 | 0 | 0 |
| Hi-flow bypass rate (cum/sec) | 1.84 | 0.46 | 0.25 |
| Flow Transfer Function | | | |
| Input (cum/sec) | 0 | 0 | 0 |
| Output (cum/sec) | 0 | 0 | 0 |
| Input (cum/sec) | 10 | 10 | 10 |
| Output (cum/sec) | 10 | 10 | 10 |
| Gross Pollutant Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (kg/ML) | 0 | 0 | 0 |
| Output (kg/ML) | 0 | 0 | 0 |
| Input (kg/ML) | 100 | 100 | 100 |
| Output (kg/ML) | 2 | 2 | 2 |
| Total Nitrogen Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 50 | 50 | 50 |
| Output (mg/L) | 50 | 50 | 50 |
| Total Phosphorus Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 0.5 | 0.5 | 0.5 |
| Output (mg/L) | 0.5 | 0.5 | 0.5 |
| Input (mg/L) | 10 | 10 | 10 |
| Output (mg/L) | 7 | 7 | 7 |
| Total Suspended Solids Transfer Function | | | |
| Enabled | TRUE | TRUE | TRUE |
| Input (mg/L) | 0 | 0 | 0 |
| Output (mg/L) | 0 | 0 | 0 |
| Input (mg/L) | 75 | 75 | 75 |
| Output (mg/L) | 75 | 75 | 75 |
| Input (mg/L) | 1000 | 1000 | 1000 |
| Output (mg/L) | 300 | 300 | 300 |
| TSS Flow based Efficiency Enabled | Off | Off | Off |
| TSS Flow based Efficiency | | | |
| TP Flow based Efficiency Enabled | Off | Off | Off |
| TP Flow based Efficiency | | | |
| TN Flow based Efficiency Enabled | Off | Off | Off |
| TN Flow based Efficiency | | | |
| GP Flow based Efficiency Enabled | Off | Off | Off |
| GP Flow based Efficiency | | | |



Table B-16: Other nodes – TWG stormwater consultant - East cluster

| | | | | Pond | | | | | | | | | | |
|-----------|-----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | H02a_LO | E01_LOT_ | 29+30+31 | E02_LOT_ | Pond 28 | | Ropes | | E01 Trunk | E02 Trunk | E03 Trunk | | |
| Location | 1 | T_Jnc | Jnc | Report | Jnc | Report | Junction | Creek | OUTLET | Drainage | Drainage | Drainage | | |
| ID | 32 | 33 | 34 | 35 | 36 | 5 37 | 38 | 39 | 40 | 46 | 48 | 50 | 52 | 56 |
| Node Type | JunctionN | Junction | Junction | Junction | Junction | Junction | JunctionN |



B.3 MUSIC model water balances

B.3.1 Northwest cluster

Table B-17 - MUSIC Water Balance Summary - Sydney Water - Northwest cluster

| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|--------------------------|---|--------------|---------------|----------|-------------------|---|
| In | Rainfall (precipitation) | 206.6 | 0.69 | m/yr. | 1,424.3 | Total Precinct - Modelled from 1999 to 2008 in MUSIC |
| In | Harvested stormwater (Recycled water supply) | NA | 353.4 | ML/yr. | 353.4 | Based on MUSIC modelling |
| In | Remaining recycled water supply (waste or potable water) | NA | 13.2 | ML/yr. | 13.2 | Meeting recycled water demand shortfall from stormwater |
| Total In | | 1,790.9 | | | | |
| Recycled water use | Internal recycled water demand | 170.5 | 3.8 | kL/Nha/d | 236.5 | Sydney Water figures for internal use demand (3.8kL/day per hectare of net developable land). Daily re-use demand from MUSIC model |
| Irrigation Demand | Irrigation recycled water demand (on-lot, street verge, public open space, Sydney Water assets, and floodplain) | NA | 0.3 to 0.6 | m/Ha/yr. | 130.5 | Based on ability of soil to absorb water without impact salinity or vegetation health. Annual demand value from MUSIC model |
| Total recy | cled water use | | | | 370.0 | |
| Out | Soil infiltration/ Absorption on lot | 140.6 | 0.0013 | m/yr. | 1.8 | Rainfall only. Irrigation not known. This was taken as all |



| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|-----------|---|--------------|--------|-------|-------------------|--|
| | | | | | | deep seepage loss and baseflow out of all lot source nodes in the MUSIC model |
| | Soil infiltration/ Absorption public open space | 77.6 | 0.0045 | m/yr. | 3.5 | Rainfall only. Irrigation not known. This was taken as all infiltration loss, seepage loss, and baseflow out from all non-lot source nodes and all treatment nodes |
| Out | Creek flows (flows not harvested) | 206.6 | 0.21 | m/yr. | 428 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from land | 206.2 | 0.25 | m/yr. | 518.3 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from basins | 11.6 | 1.2 | m/yr. | 139.3 | Based on MUSIC modelling. Area taken as area of all attached treatment nodes |
| Total Out | | | | | 1,090.9 | |



Table B-18 - MUSIC Water Balance Summary – TWG stormwater consultant - Northwest cluster

| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|--------------------------|---|--------------|---------------|----------|-------------------|---|
| In | Rainfall (precipitation) | 207.7 | 0.69 | m/yr. | 1,435.2 | Total Precinct - Modelled from 1999 to 2008 in MUSIC |
| In | Harvested stormwater (Recycled water supply) | NA | 371.3 | ML/yr. | 371.3 | Based on MUSIC modelling |
| In | Remaining recycled water supply (waste or potable water) | NA | 5.7 | ML/yr. | 5.7 | Meeting recycled water demand shortfall from stormwater |
| Total In | | | | | 1,812.2 | |
| Recycled water use | Internal recycled water demand | 170.5 | 3.8 | kL/Nha/d | 236.5 | Sydney Water figures for internal use demand (3.8kL/day per hectare of net developable land). Daily re-use demand from MUSIC model |
| Irrigation Demand | Irrigation recycled water demand (on-lot, street verge, public open space, Sydney Water assets, and floodplain) | NA | 0.3 to 0.6 | m/Ha/yr. | 140.7 | Based on ability of soil to absorb water without impact salinity or vegetation health. Annual demand value from MUSIC model |
| Total recy | cled water use | 377.2 | | | | |
| Out | Soil infiltration/ Absorption on lot | 140.6 | 0.0013 | m/yr. | 1.8 | Rainfall only. Irrigation not known. This was taken as all deep seepage loss and baseflow out of |



| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|-----------|---|--------------|--------|-------|-------------------|--|
| | | | | | | all lot source nodes in the MUSIC model |
| | Soil infiltration/ Absorption public open space | 75.9 | 0.0049 | m/yr. | 3.7 | Rainfall only. Irrigation not known. This was taken as all infiltration loss, seepage loss, and baseflow out from all non-lot source nodes and all treatment nodes |
| Out | Creek flows (flows not harvested) | 207.7 | 0.21 | m/yr. | 423 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from land | 207.7 | 0.26 | m/yr. | 537.3 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from basins | 8.8 | 1.2 | m/yr. | 107.4 | Based on MUSIC modelling. Area taken as area of all attached treatment nodes |
| Total Out | | | | | 1,073.2 | |



B.3.2 East cluster

Table B-19 - MUSIC Water Balance Summary - Sydney Water - East cluster

| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|--------------------------|---|--------------|---------------|----------|-------------------|---|
| In | Rainfall (precipitation) | 236.2 | 0.69 | m/yr. | 1,632 | Total Precinct - Modelled from 1999 to 2008 in MUSIC |
| In | Harvested stormwater (Recycled water supply) | NA | 304.7 | ML/yr. | 304.7 | Based on MUSIC modelling |
| In | Remaining recycled water supply (waste or potable water) | NA | 15.3 | ML/yr. | 15.3 | Meeting recycled water demand shortfall from stormwater |
| Total In | | 1,952 | | | | |
| Recycled water use | Internal recycled water demand | 162.6 | 3.8 | kL/Nha/d | 225.6 | Sydney Water figures for internal use demand (3.8kL/day per hectare of net developable land). Daily re-use demand from MUSIC model |
| Irrigation Demand | Irrigation recycled water demand (on-lot, street verge, public open space, Sydney Water assets, and floodplain) | NA | 0.3 to 0.6 | m/Ha/yr. | 94.0 | Based on ability of soil to absorb water without impact salinity or vegetation health. Annual demand value from MUSIC model |
| Total recy | cled water use | | | | 319.6 | |
| Out | Soil infiltration/ Absorption on lot | 149.8 | 0.0013 | m/yr. | 1.9 | Rainfall only. Irrigation not known. This was taken as all deep seepage loss and baseflow out of |



| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|-----------|---|--------------|--------|-------|-------------------|--|
| | | | | | | all lot source nodes in the MUSIC model |
| | Soil infiltration/ Absorption public open space | 101.0 | 0.0057 | m/yr. | 5.8 | Rainfall only. Irrigation not known. This was taken as all infiltration loss, seepage loss, and baseflow out from all non-lot source nodes and all treatment nodes |
| Out | Creek flows (flows not harvested) | 236.2 | 0.20 | m/yr. | 464 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from land | 236.2 | 0.30 | m/yr. | 707.2 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from basins | 14.6 | 1.1 | m/yr. | 160.9 | Based on MUSIC modelling. Area taken as area of all attached treatment nodes |
| Total Out | | | | | 1,339.8 | |



Table B-20 - MUSIC Water Balance Summary – TWG stormwater consultant - East cluster

| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|--------------------------|---|--------------|---------------|----------|-------------------|---|
| In | Rainfall (precipitation) | 239.3 | 0.69 | m/yr. | 1,653.4 | Total Precinct - Modelled from 1999 to 2008 in MUSIC |
| In | Harvested stormwater (Recycled water supply) | NA | 291.2 | ML/yr. | 291.2 | Based on MUSIC modelling |
| In | Remaining recycled water supply (waste or potable water) | NA | 16.0 | ML/yr. | 16.0 | Meeting recycled water demand shortfall from stormwater |
| Total In | | - | <u>.</u> | | 1,960.6 | |
| Recycled water use | Internal recycled water demand | 154.0 | 3.8 | kL/Nha/d | 213.6 | Sydney Water figures for internal use demand (3.8kL/day per hectare of net developable land). Daily re-use demand from MUSIC model |
| Irrigation Demand | Irrigation recycled water demand (on-lot, street verge, public open space, Sydney Water assets, and floodplain) | NA | 0.3 to 0.6 | m/Ha/yr. | 94.0 | Based on ability of soil to absorb water without impact salinity or vegetation health. Annual demand value from MUSIC model |
| Total recy | cled water use | 307.6 | | | | |
| Out | Soil infiltration/ Absorption on lot | 141.3 | 0.0013 | m/yr. | 1.8 | Rainfall only. Irrigation not known. This was taken as all deep seepage loss and baseflow out of |



| Flux | Water sources | Area (Ha) | Rate | Unit | Volume (ML/yr) | Assumptions or comments |
|-----------|---|--------------|--------|-------|-------------------|--|
| | | | | | | all lot source nodes in the MUSIC model |
| | Soil infiltration/ Absorption public open space | 110.1 | 0.0083 | m/yr. | 9.1 | Rainfall only. Irrigation not known. This was taken as all infiltration loss, seepage loss, and baseflow out from all non-lot source nodes and all treatment nodes |
| Out | Creek flows (flows not harvested) | 239.3 | 0.20 | m/yr. | 468 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from land | 239.3 | 0.32 | m/yr. | 761.9 | Based on MUSIC modelling. Area taken as area of all attached source nodes |
| Out | Evaporative losses from basins | 12.1 | 1.1 | m/yr. | 133.9 | Based on MUSIC modelling. Area taken as area of all attached treatment nodes |
| Total Out | | | | | 1,374.7 | |